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SL-7-18

RADAR AND TUCKER WAVEMETER DATA
FROM SEA-LAND McLEAN
VOYAGE 34

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SHIP STRUCTURE COMMITTEE 1978

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Project SR-1221

"Correlation and Verification of Wavemeter Data from the SL-7"

RADAR AND TUCKER WAVEMETER DATA

FROM SEA-LAND McLEAN
VOYAGE 34

by

J. F. Dalzell

Stevens Institute of Technology

under

Department of the Navy
Naval Ship Engineering Center
Contract No. NOO24-74-C-5451

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U.S. Coast Guard Headquarters Washington, D.C. 1978

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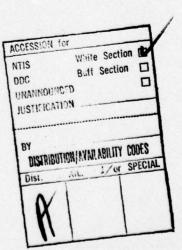
ABSTRACT

So that more precise correlations between full scale observations and analytical and model results could be carried out, one of the objectives of the instrumentation program for the SL-7 class container ships was the provision of instrumental measures of the wave environment. To this end, two wave meter systems were installed on the S.S. SEA-LAND McLEAN. Raw data was collected from both systems during the second (1973-1974) and third (1974-1975) winter data collecting seasons.

It was the purpose of the present work to reduce this raw data, to develop and implement such corrections as were found necessary and feasible, and to correlate and evaluate the final results from the two wave meters. In carrying out this work it was necessary to at least partly reduce several other channels of recorded data, so that, as a by-product, reduced results were also obtained for midship bending stresses, roll, pitch, and two components of acceleration on the ship's bridge.

As the work progressed it became evident that the volume of documentation required would grow beyond the usual dimensions of a single technical report. For this reason the analyses, the methods, the detailed results, discussions, and conclusions are contained in a series of ten related reports.

This report is one of the six in the series in which the detailed results of the data reduction process are presented. Included in this report is the reduced data from the Second Season Voyage 34.



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INTRODUCTION

It was one of the objectives of the SL-7 full-scale instrumentation program to provide a direct instrumental measure of the wave environment so that more precise correlations could be made between full-scale observations, and analytical and model results. To this end the ship was fitted with a micro-wave radar relative wave meter and various motion sensing devices. A "Tucker Meter" pressure actuated wave height sensing system was also installed.

The purpose of the present project is to reduce and analyze the resulting radar and Tucker meter data obtained on the SEA-LAND McLEAN in the second (1973-1974) and third (1974-1975) winter recording seasons. The purpose of the present report is to present the reduced data from the Second Season Voyage 34.

BACKGROUND

Since the purpose of the present report is only to document a portion of the reduced data, it should be noted that details of the experiments themselves, and of the analyses leading up to the present results, are contained elsewhere. To be specific, References 1 and 2 contain, for both recording seasons in question, a full account of the instrumentation, basic recording, and the nominal circumstances surrounding the present data. References 3 and 5 contain the detail of the reduction of the original data to digital form. Reference 4 contains the detail of the analyses and of the procedures used in generating the present results. Finally, Reference 6 contains the summary, discussion and conclusions.

NOTES ON THE CONTENTS

Each voyage leg was processed, and is presented, as a unit. The first part of the presentation for each voyage leg is a four-part table.

Parts a and b of each table contain the log-book data extracted from Ref. 1 or 2. With the exception of the first column of each page, the meaning of each entry is that established by Teledyne Materials Research. The first column is the run number assigned to each interval during the digitization at D.L. This number is retained for identification throughout.

Part c of each table is a comparison of results from the present digitization with that at TMR. Five columns are stress results obtained at TMR. Stresses are presented in thousands of pounds per square inch. The columns marked 6 through 8 are from the present digitization. Column 6 "range of recorded extremes" was computed from the first pass analysis by scaling the extremes in each interval and subtracting the smallest extreme from the largest. Column 7 is $2\sqrt{2}$ times the process rms. This estimate should compare with the value given by TMR for "rms P to T stress,". Column 8 is the difference of the sample mean of the interval noted, from the sample mean of the first interval digitized in each voyage leg. The remaining columns are various ratios of present results to those obtained by TMR.

Part d of the tables involves indices of the magnitude of <u>raw</u> radar, roll, pitch, vertical and transverse acceleration, and Tucker meter signals. The first index in each case is 4.0 x the rms. The second and third indices are the positive and negative extremes for each channel. The extremes observed for roll and pitch were corrected for electrical zero on tape before scaling. The extremes for all other items were corrected to the sample mean before scaling. The senses of pitch and Tucker meter are not correct for reasons noted in Ref. 4, and it is to be emphasized that all data is raw (uncorrected for anything).

The second part of the presentation for each voyage leg is a series of charts, a pair of charts for each interval. The first of the pair includes plots of spectra of midship vertical bending stress, roll, corrected radar wave elevation, Tucker meter wave, and the mean dynamic head at frame 119. The "mean dynamic head" is a partial correction of the Tucker meter as detailed in Ref. 4. At the left of the first chart is a tabulation of various data; portions of the log book data from the tables, two indices of midship stress, a summary of the magnitude of motions,

and finally a table summarizing wave height statistics obtained from spectra as well as peak-trough analyses of the time histories.

The second chart of the pair for each interval are sample time histories for five of the channels of information treated in the first chart. As noted in Reference 4, there was at the end of data reduction 16-1/2 minutes of valid radar wave elevation data. To produce the charts an 8-1/2 minute portion of this sample was selected.

A fuller discussion of the background and conventions employed in the charts is presented in the Appendix.

REFERENCES

- Wheaton, J.W. and Boentgen, R.R., "Second Season Results from Ship Response Instrumentation Aboard the SL-7 Class Containership S.S. SEA-LAND McLEAN in North Atlantic Service," SL-7-9, 1976, AD-A034162.
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- Dalzell, J.F., "Original Radar and Standard Tucker Wavemeter SL-7 Containership Data Reduction and Correlation Sample," SSC-277, SL-7-14. 1978.
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- 6. Dalzell, J.F., "Results and Evaluation of the SL-7 Containership Radar and Tucker Wavemeter Data," SSC-280, SL-7-23. 1978.

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TABLE la

SUMMARY OF TMR LOG-BOOK DATA CORRESPONDING TO INTERVALS SELECTED FOR WAVE METER DATA REDUCTION (PAGE 1 OF 2)

SEA LAND MC LEAN : 1973-1974 WINTER SEASON : UDYAGE 34 EAST

SEA/AIR TEMP	45/45	45/45	64/49	65/52	59/55	58/52	09/99	65/55	34/44	57/52	60/55	57/48	56/46	55/45	54/47	53/60	53/50	52/54	52/50	52/45	51/47	51/48	53/44	50/47
DRAFT FT.	29.80	30.10	30.08	30,11	30.08	30.02	30.00	30.00	30.00	30.05	30.08	30.10	30.10	30.09	30.05	30.09	30.00	29.89	29.75	29.62	29.57	29.61	29,75	29.80
PROP	132.0	131.7	132.0	131,8	131.3	131,8	131.5	130.1	131.7	133.1	132.2	131.0	132.2	130.0	132.0	132.0	132.6	132.0	133.0	132.5	133.0	132.0	131.2	131.6
SPEED KT.											32.3	32.1	32.3	31.8	32.3	32.3	32.4	32.3	32.6	32.4	32.6	32.3	32.1	32.2
COURSE	082	680	087	060	060	060	060	060	060	060	073	073	073	073	073	072	072	072	072	071	071	071	071	071
LONGITUDE				59-02 W	59-02 W	59-02 W	59-02 W	1	59-02 W	43-08 W	43-08 W	43-08 W	1	43-08 W	43-08 W	1	27-18 W	1	27-18 W	1	1	1	10-20 W	10-20 W
LATITUDE				40-31 N	1	40-31 N	40-31 N	40-31 N	40-31 N	29	40-59 N		29	T.	40-59 N	27	-27	-27		-27	1	-10	0	48-10 N
TIME (GMT) LATITUDE	2400	0400	0800	40-	40-	1	2400 40-31 N	40-	40-	40-59	29	40-59	40-59	26	40-59	-27	44-27	44-27	-27	44-27	44-27	0	48-10	2000 48-10 N
	-29-74	-30-74	-30-74	-30-74 1200 40-	-30-74 1600 40-	-30-74 2000 40-	-30-74 2400 40-	-31-74 0400 40-	-31-74 0800 40-	-31-74 1200 40-59	-31-74 1600 40-59	40-59	-31-74 2400 40-59	-01-74 0400 40-59	-01-74 0800 40-59	-01-74 1200 44-27	-01-74 1600 44-27	-01-74 2000 44-27	-01-74 2400 44-27	-02-74 0400 44-27	-02-74 0800 44-27	-02-74 1200 48-10	-02-74 1600 48-10	-02-74 2000 48
TIME TE (GMT)	01-29-74	01-30-74	01-30-74	01-30-74 1200 40-	01-30-74 1600 40-	01-30-74 2000 40-	01-30-74 2400 40-	01-31-74 0400 40-	01-31-74 0800 40-	01-31-74 1200 40-59	01-31-74 1600 40-59	-31-74 2000 40-59	01-31-74 2400 40-59	02-01-74 0400 40-59	02-01-74 0800 40-59	02-01-74 1200 44-27	02-01-74 1600 44-27	02-01-74 2000 44-27	02-01-74 2400 44-27	02-02-74 0400 44-27	02-02-74 0800 44-27	02-02-74 1200 48-10	02-02-74 1600 48-10	02-02-74 2000 48
TIME DATE (GMT)	9 01-29-74	13 01-30-74	17 01-30-74	21 01-30-74 1200 40-	26 01-30-74 1600 40-	29 01-30-74 2000 40-	33 01-30-74 2400 40-	37 01-31-74 0400 40-	41 01-31-74 0800 40-	45 01-31-74 1200 40-59	49 01-31-74 1600 40-59	01-31-74 2000 40-59	5 01-31-74 2400 40-59	9 02-01-74 0400 40-59	13 02-01-74 0800 40-59	17 02-01-74 1200 44-27	22 02-01-74 1600 44-27	25 02-01-74 2000 44-27	29 02-01-74 2400 44-27	34 02-02-74 0400 44-27	37 02-02-74 0800 44-27	41 02-02-74 1200 48-10	45 02-02-74 1600 48-10	49 02-02-74 2000 48
TMR INTO TATE (GMT)	9 01-29-74	4 13 01-30-74	5 17 01-30-74	6 21 01-30-74 1200 40-	7 26 01-30-74 1600 40-	8 29 01-30-74 2000 40-	9 33 01-30-74 2400 40-	10 37 01-31-74 0400 40-	11 41 01-31-74 0800 40-	12 45 01-31-74 1200 40-59	13 49 01-31-74 1600 40-59	14 1 01-31-74 2000 40-59	15 5 01-31-74 2400 40-59	16 9 02-01-74 0400 40-59	17 13 02-01-74 0800 40-59	18 17 02-01-74 1200 44-27	19 22 02-01-74 1600 44-27	20 25 02-01-74 2000 44-27	21 29 02-01-74 2400 44-27	22 34 02-02-74 0400 44-27	23 37 02-02-74 0800 44-27	24 41 02-02-74 1200 48-10	25 45 02-02-74 1600 48-10	26 49 02-02-74 2000 48
TMR TMR INDX INTO NO. DATE (GMT)	157 3 9 01-29-74	157 4 13 01-30-74	157 5 17 01-30-74	157 6 21 01-30-74 1200 40-	157 7 26 01-30-74 1600 40-	157 8 29 01-30-74 2000 40-	157 9 33 01-30-74 2400 40-	157 10 37 01-31-74 0400 40-	157 11 41 01-31-74 0800 40-	157 12 45 01-31-74 1200 40-59	157 13 49 01-31-74 1600 40-59	14 1 01-31-74 2000 40-59	159 15 5 01-31-74 2400 40-59	159 16 9 02-01-74 0400 40-59	159 17 13 02-01-74 0800 40-59	159 18 17 02-01-74 1200 44-27	159 19 22 02-01-74 1600 44-27	159 20 25 02-01-74 2000 44-27	159 21 29 02-01-74 2400 44-27	159 22 34 02-02-74 0400 44-27	159 23 37 02-02-74 0800 44-27	159 24 41 02-02-74 1200 48-10	159 25 45 02-02-74 1600 48-10	159 26 49 02-02-74 2000 48

TABLE 1b

SUMMARY OF TMR LOG-BOOK DATA CORRESPONDING TO INTERVALS SELECTED FOR WAVE METER DATA REDUCTION (PAGE 2 OF 2)

SEA LAND MC LEAN : 1973-1974 WINTER SEASON : UDYAGE 34 EAST

COMMENTS		
VISUAL WEATHER /TMR LOG-BOOK COMMENTS		
/TAR		
WEATHER		1
VISUAL	CLEAR / CLEAR / CCCAST / OCCAST /	PT CLDY
<-SWELL-> HT LENGTH FT. FT.	150 150 150 150 150 150 150 150 150 150	300
^-SW HT L FT.	01 W 4 4 W N N N N W W W W W W W W W W W W	-
REL SWELL DIR	172P 177P 177P 180 180 180 180 152S 152S 152S 152S 152S 63S 63S 63S 64S 64S	648
MAVE HT.		-
MAVE DIR	172P 179P 199P 111S 111S 22S 111S 22S 111S 955P 955P 955P 1177P 117P 117P 117P 117P 117P 117P 117P 117P 117P 117P 117P 117P 117P 117	1548
<pre><rel wind=""> DIR/SPEED /(KT)</rel></pre>	172P/ 5 179P/ 5 19P/ 5 0 / 5 0 / 5 115/ 8 115/ 8 455/12 225/12 225/12 115/ 5 95P/ 5 95P/ 5 95P/ 15 117P/20 117P/20 151P/30 117P/30 151P/30 161P/20 161P/20 161P/20	1545/10
SEA	000000044000044400CC00000	10
B.L. RUN NO. S	1009 10013 10017 10026 10029 10037 10045 11001 11009 11103 11122 11123 11137 11137 11137 11137	1149

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TABLE 1c

COMPARISON OF TMR RESULTS FOR MIDSHIP VERTICAL BENDING STRESS WITH CORRESPONDING RAW DIGITIZATION RESULTS AT DAVIDSON LABORATORY

SEA LAND MC LEAN : 1973-1974 WINTER SEASON : UOYAGE 34 EAST

ATI0S-		(9)	`	`			1.1		1.4		1.8		9 1.11	-	1.	95 1.20	-	-	-	-	-		-	37 1.53	1.	0	60 1.41	4 1.14	3 1.2	1
UMN		(9)	-	(3+5)			-	-	-	-	-	-	0.89	-	+	0	-		1.43			0.80	1.	-	1.	0	0	-	1.2	1.
cor		(2)	,	(4)			1.21	1.20	1,41	1.51	1.48	1.33	1.22	1.21	1,15	1.07	1.30	1.19	1.35	1,34	1.23	1.20	1.34	1.23	1.34	1.14	1,22	1.22	1.14	1.19
*	*	*	×s	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	_	*	*	*	*
NOI	REL	MEAN	STRES	KPSI	* (8)		-1.93		-2.22	1.53	+	1.40	0.33		0.59	0.74		0.91	69.0	0.87	0.82	1.50	1.64		2.04	1.73	1,80	1.90	1.86	1.89
DIGITIZATION>* <column ratios=""></column>		8)			(2)		1.40		2.27		2.12	1.96	2.04	2.24	2.61	3.78	3.15	3.28	3.67	3.92	3.48	3,32	3.94	4.00	3.80	3.85	3.65	4.30		3.39
<b.l.< th=""><th>RANGE OF</th><th>RECORDED</th><th>EXTREMES</th><th>KPSI</th><th></th><th></th><th>3.18</th><th></th><th>10</th><th></th><th></th><th>4.95</th><th>4.70</th><th>5.44</th><th>5.88</th><th>8.90</th><th>8.37</th><th>7.72</th><th>9.37</th><th>8.80</th><th>8.04</th><th>8.31</th><th>9.37</th><th>9.83</th><th>9.35</th><th>7.64</th><th>9.20</th><th>7.88</th><th></th><th>5.46</th></b.l.<>	RANGE OF	RECORDED	EXTREMES	KPSI			3.18		10			4.95	4.70	5.44	5.88	8.90	8.37	7.72	9.37	8.80	8.04	8.31	9.37	9.83	9.35	7.64	9.20	7.88		5.46
*	*	*	×s	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
1																														
1	2		STRES				00.0	00.0	00.0	00.0	00.0	00.0	1.05		0.67	1.91	00.00	1.14	1.20		+	1.58			00.0		8.74	00.0		00.0
	2	_	STRES				0.	0	0	0	0	0		98	27	53		75 1.	71 1.	92 1.	84 1.	77 1.	94 1.	26 0.	84 0.	38 0.	8.7	0	.0 06	
· ESUL TS	MAX RMS P	T-0T- P-T0-T	STRESS STRES	KPSI	(4)		.79 1.15 0.	.74 1.54 0.	61 0.	.15 1.12 0.	.77 1.43 0.	.40 1.47 0.	67 1.	.73 1.86 0.	.52 2.27	3.53	.84 2.41	71 2.75 1.	2.71 1.	36 2.92 1.	58 2.84 1.	2.77 1.	28 2.94 1.	41 3.26 0.	92 2.84 0.	04 3.38 0.	50 2.98 8.7	54 0.	71 3.90 0.	.86 0.
TMR RESULTS	MAX RMS P	P-T0-T P-T0-T	STRESS STRESS STRES	STS KPSI KPSI	(3) (4)		2.79 1.15 0.	.74 1.54 0.	3.74 1.61 0.	.15 1.12 0.	2.77 1.43 0.	3.40 1.47 0.	4.25 1.67 1.	3.73 1.86 0.	4.52 2.27	7.44 3.53	4.84 2.41	7.71 2.75 1.	5.34 2.71 1.	6.36 2.92 1.	1 6.58 2.84 1.	8.77 2.77 1.	7.28 2.94 1.	6.41 3.26 0.	6.92 2.84 0.	8.04 3.38 0.	6.50 2.98 8.7	92 3.54 0.	7.71 3.90 0.	.32 2.86 0.
TMR RES	MAX RMS P	1ST P-T0-T P-T0-T	MODE STRESS STRESS STRES	KPSI KPSI	(3) (4)		0 2.79 1.15 0.	0 3.74 1.54 0.	0 3.74 1.61 0.	0 2.15 1.12 0.	0 2.77 1.43 0.	0 3.40 1.47 0.	19 4.25 1.67 1.	13 3.73 1.86 0.	2 4.52 2.27	21 7.44 3.53	0 4.84 2.41	8 7.71 2.75 1.	12 5.34 2.71 1.	15 6.36 2.92 1.	11 6.58 2.84 1.	10 8.77 2.77 1.	3 7.28 2.94 1.	1 6.41 3.26 0.	0 6.92 2.84 0.	4 8.04 3.38 0.	1 6.50 2.98 8.7	6.92 3.54 0.	0 7.71 3.90 0.	0 4.32 2.86 0.
TMR RES	NO. NO. MAX RMS P	WAVE 1ST P-TO-T P-TO-T	*INDUCED MODE STRESS STRES	BURSTS KPSI KPSI) (2) (3) (4)	*	* 109 0 2.79 1.15 0.	* 86 0 3.74 1.54 O.	* 95 0 3.74 1.61 0.	* 109 0 2.15 1.12 O.	* 93 0 2.77 1.43 0.	* 108 0 3.40 1.47 O.	* 127 19 4.25 1.67 1.	* .128 13 3.73 1.86 0.	* 128 2 4.52 2.27	* 142 21 7.44 3.53	* 108 0 4.84 2.41	* 108 8 7.71 2.75 1.	* 105 12 5.34 2.71 1.	* 106 15 6.36 2.92 1.	* 109 11 6.58 2.84 1.	* 93 10 8.77 2.77 1.	* 94 3 7.28 2.94 1.	* 69 1 6.41 3.26 0.	* 90 0 6.92 2.84 O.	* 79 4 8.04 3.38 O.	* 64 1 6.50 2.98 8.7	0 6.92 3.54 0.	* 49 0 7.71 3.90 0.	* 24 0 4.32 2.86 0.

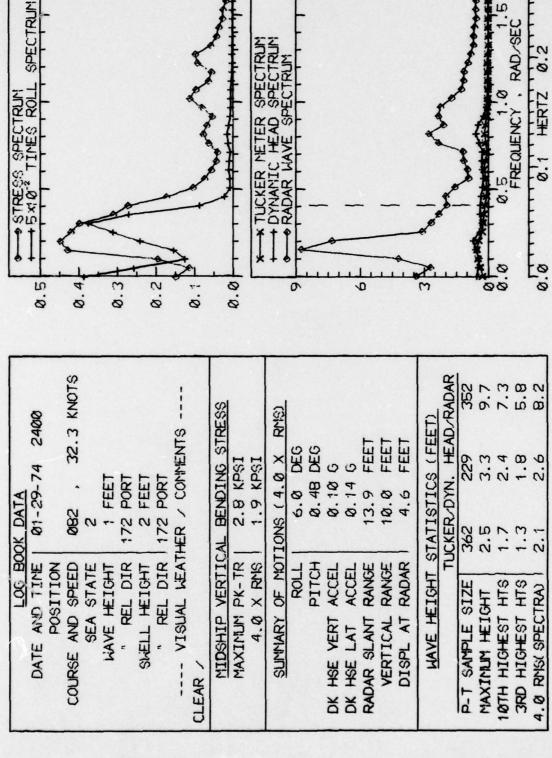
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TABLE 14

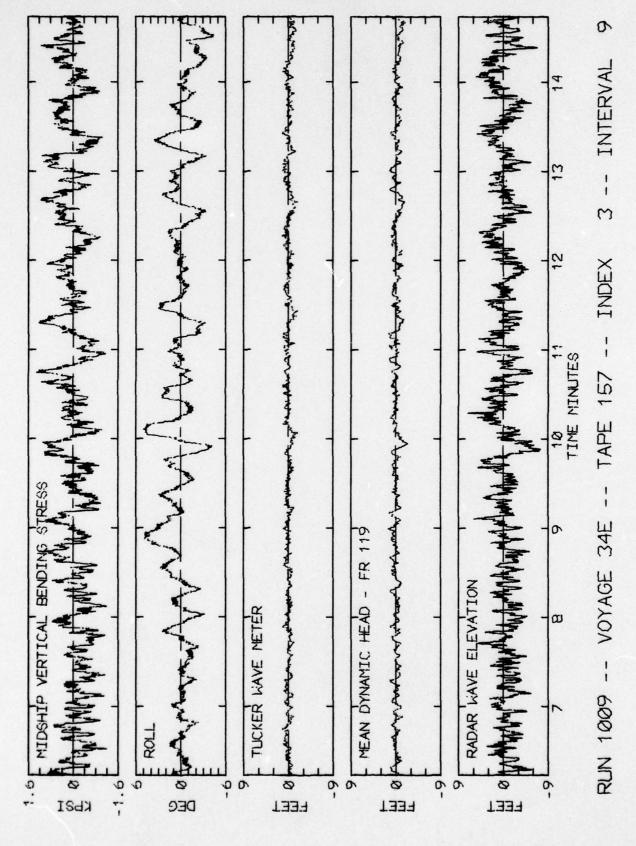
SUMMARY OF RAW DIGITIZATION RESULTS FOR RADAR RANGE ROLL, PITCH, DECK HOUSE ACCELERATIONS, AND TUCKER METER

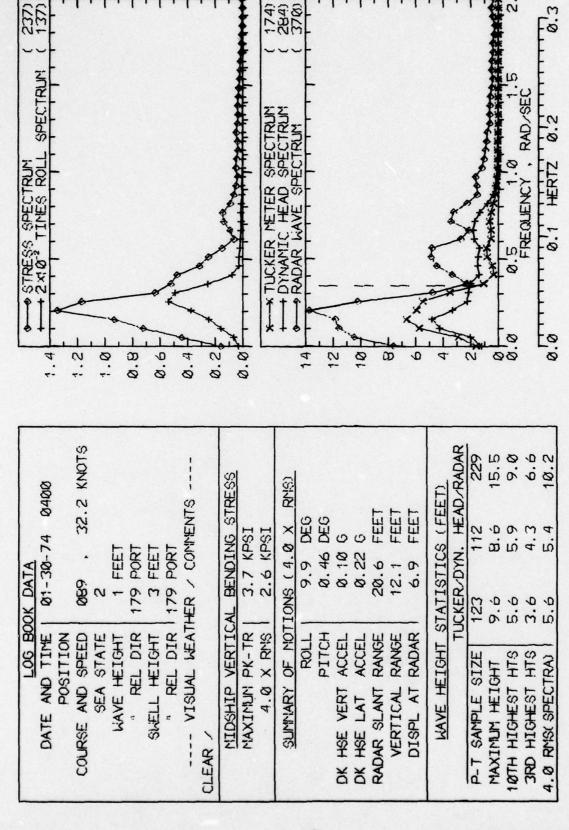
SEA LAND MC LEAN : 1973-1974 WINTER SEASON : VOYAGE 34 EAST

KER> RECORDED EXTREMES	FI	-2.	-3.	-3.	-2.	-3.	-2.	-3.	-4.	-4.	-6.	-4.	-5.	-5	-5.	-5	-5	-6.	-6.	-7.	-6-	-10.	8	-11.	-11.
TUCKER O RECO S) EXTR	FT	2	7.	ů,	3	4	4	4	4	4	4	5	• 9	7.	ů.	8	6	7.	7.	10.	10.	11.	11:	11.	11.
4 8	FT	2	• 9	4.	3	4.	4	4.	4.	ים	• 9	i,	• 9	• •	.9	• •	6	8	8	12.	14.	15.	17.	16.	18.
ACCEL>< RECORDED EXTREMES	(9)	-0.1	-0.2	-0.2	-0.1	-0.2	-0.2	-0.1	-0.2		-0.2	-0.2	-0.2	-0.3	-0.2		-0.3	4.0-	4.0-	-0.3	4.0-	-0.4	4.0-	-0.4	-0.2
REC	(9)	0.1	0.2	0.2	0	0.2		0.2	0.2	0.1	0.2	0.2		0.3	0.2	0.3		0.2	0.3	0.3	0.3		0.3	4.0	0.2
4.0 (RMS)		0.14	0.22	0.21	0.13	0.19	0.18	0.16	0.20		0.22	0.27	0.28	0:30	0.30		0.35	0.34	0.39	0.41	0.42	0.43	0.46	0.51	0.27
ACCEL->< RECORDED EXTREMES	(9)	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.2			-0.2	-0.2		-0.2		-0.2			-0.2		-0.2	-0.1	-0.1	0.0-
OK III	(9)	0.1	0.1		0.1	0.1		0.1	0.2			0.2	N		0.2		0.2	0.2	•	0.3	0.2	0.2	0.1	0.1	0.0
VERT 4.0 (RMS)		0.10	0.10	0.10	0.08	0.10	0.12		0.19		0.39	0.26		0.25	0.23			0.23		0.26	0.26	0.18	0.14	0.10	0.04
	DEG	-1.1	•	-1.2	-1.0	-1.1	-1.2	-1.2	-1.4	-1.6	-1.9	-1.6	-1.6	•	-1.4	-1.6	-1.5	-1.3	-1.6	-1.6	-1.7	•	-1.2		-1.1
PITCH>< RECORDED > EXTREMES	DEG	0.0-	-0.1	0.0	-0.1	0.1	0.1	0.1	0.3	0.5	1.1	9.0	9.0	9.0	4.0	4.0		0.5	4	8.0	9.0	4	0.2	0.2	0.1
4.0	DEG	0.5	0.5	0.5	0.4	0.5	0.5	0.7	0.8	1.0	1.6	1.1	1.1	1.1	1.0	1.1	1.0	6.0	1.0	1.0	1.1		0.7	0.8	8.0
DLL><- RECORDED EXTREMES (DEG	-4-	-12.	-10.	-7.	-10.	-6-	-10.	-10.	-7.	-6-	-10.	-12.	-11.	-10.	-12.	-13.	-12.	-14.	-14.	-17.	-15.	-15.	-17.	-11.
ROLL -	DEG	i,	ń	ń	'n	ņ	4	'n	9	ů.	8	8	6	11.	11.			16.			17.		18.		8
4 0 × 8			6.6			8.9				8.0		12.1		13.7						18.7	19.8	19,6		23.1	13.1
NDAR>< RECORDED 4 EXTREMES (R	F	-12.	-14.	-18.	-12.	-18.	-16.	-12.	-22.	-17.	-26.	-19.	-21.	-22.	-25.	-20.	-20.	-26.	-21.	-23.	-26.	-22.	-22.	-20.	-17.
RADAR REC	FT	13.	21.	16.	16.	24.	14.	16.	16.	18.	27.	21.	21.	22.	22.	21.	22.	20.	24.	30.	23.	35.	23.	34.	21.
4.0	F	14.	21.	21.	14.	19.	18.	18.	21.	22.	30.	25.	25.	26.	26.	26.	27.	27.	29.	33.	30.	31.	30.	34.	24.
D.L.	NO.	1009	1013	1017	1021	1026	1029	1033	1037	1041	1045	1049	1101	1105	1109	1113	1117	1122	1125	1129	1134	1137	1141	1145	1149
					7																				

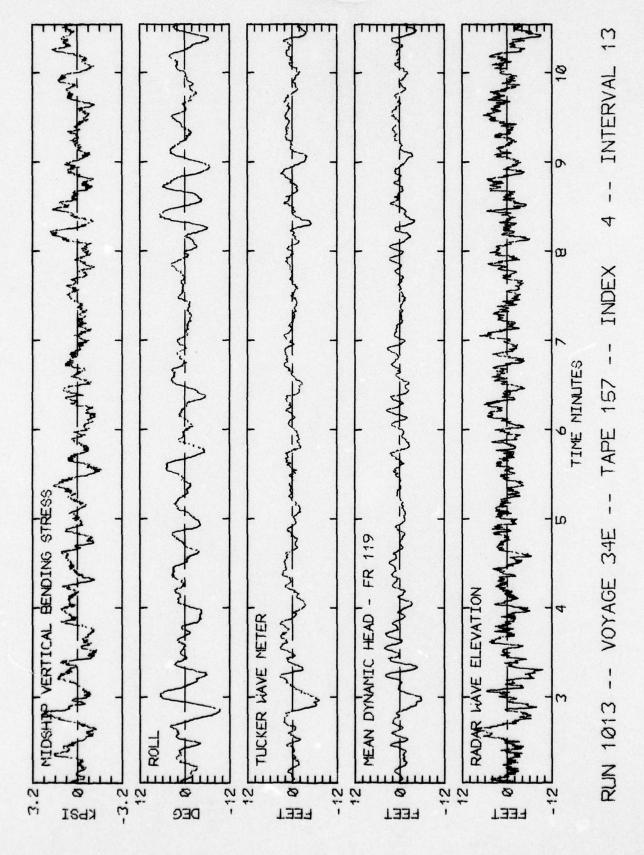


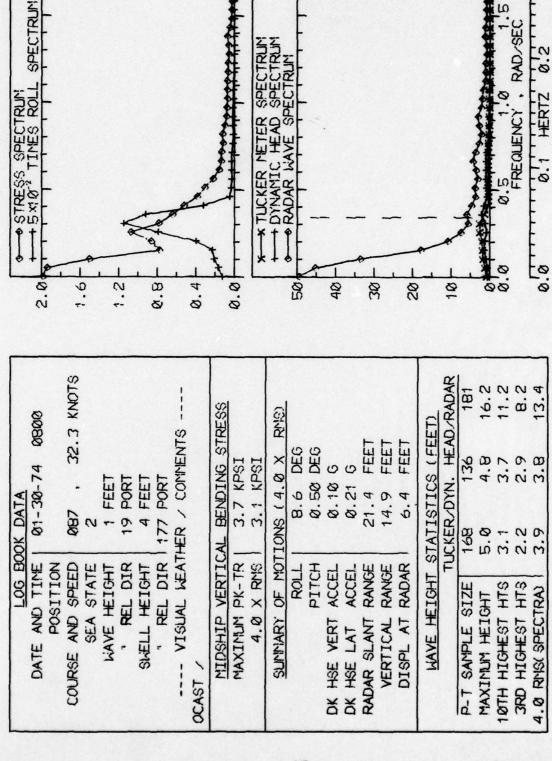
9 INTERVAL 3 --INDEX 1 -- TAPE 157 VOYAGE 34E RUN 1009 --





INTERVAL 7 -- 7 -- TAPE 157 -- INDEX RUN 1013 -- VOYAGE 34E

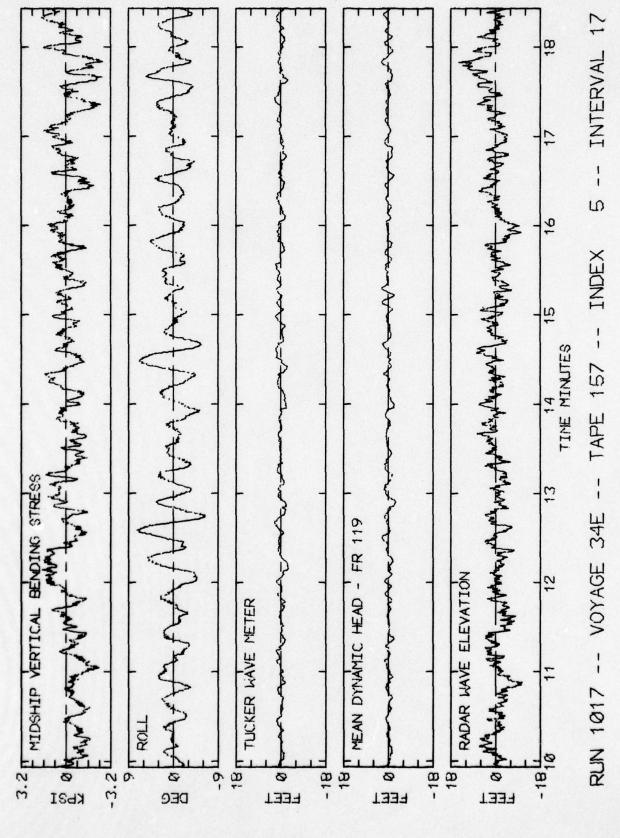




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17 INTERVAL 1 S INDEX 157 --TAPE 1 34E VOYAGE 1 RUN 1017

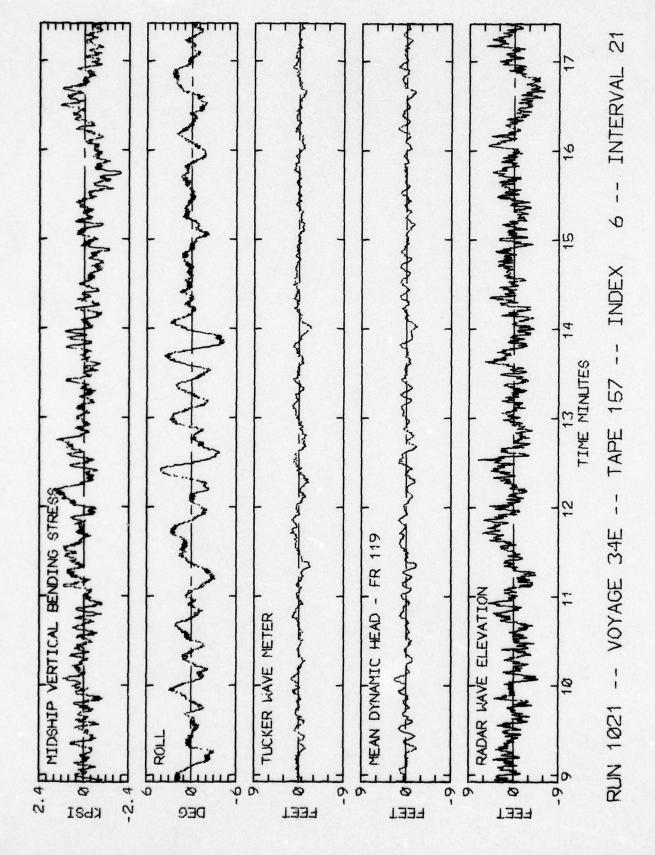
6.3

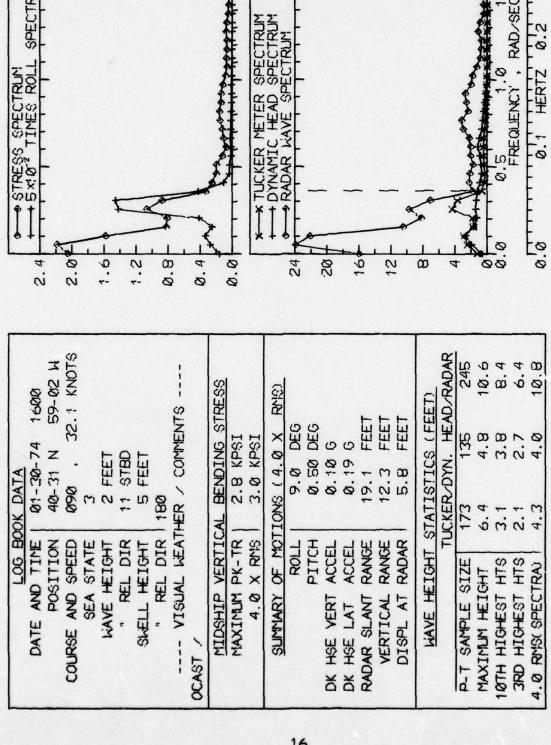


STRESS SPECTR			1.2-	- A -	++ 	V* \	\frac{1}{2}	0.45	4 B		0.0	X - X TUCKER METER	+ DYNAMIC HEAD		A	- - !			ـــ مليا م	- -		\$ L. 1. T.	A A A		0.0	FREQUENCY	0.0
DOK DATA	N 40-31 N 59-02 H	25 , 860	2	IT 2 FEET	R 8	IT 4 FEET	IR 1180	VISUAL WEATHER / COMMENTS		TICAL BENDING STRESS	R 2.1 KPSI	48 2.3 KPSI	SUMMARY OF MOTIONS (4.0 X RNS)	L 5.8 DEG		3 80.00 TE	EL 0.13 G	E 14.4 FEET	E 10.0 FEET	AR 4.2 FEET	T STATISTICS (FEET)	TUCKER/DYN. HEAD/RADAR	194 171 271	2.7 3.5 10.4	2.8 2.6 6.7		2.5 2.8 8.6
4	DATE AND TIME	COURSE AND SPEED		WAVE HEIGHT	REL DIR	SHELL HEIGHT	" REL DIR	VISUAL WE	OCAST /	MIDSHIP VERTICAL	MAXINUM PK-TR	4.0 X RMS	SUMNARY OF M	ROLL	PITCH	DK HSE VERT ACCEL	DK HSE LAT ACCEL	RADAR SLANT RANGE	VERTICAL RANGE	DISPL AT RADAR	WAVE HEIGHT		P-T SAMPLE SIZE	MAXIMUM HEIGHT	10TH HIGHEST HTS	3RD HIGHEST HTS	4.0 RMS(SPECTRA)
														1-	1												

1555 6.3 1.0 1.5 :Y , RAD/SEC :RTZ 0.2 SPECTRUM AND THE PROPERTY OF SPECTRUM SPECTRUM PECTRUM

6 -- INTERVAL 21 TAPE 157 -- INDEX RUN 1021 -- VOYAGE 34E --



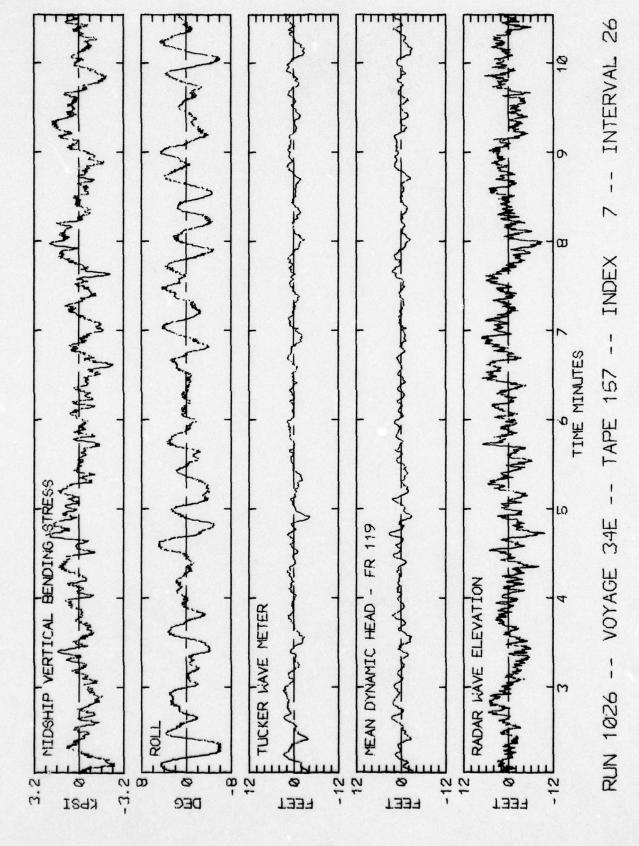


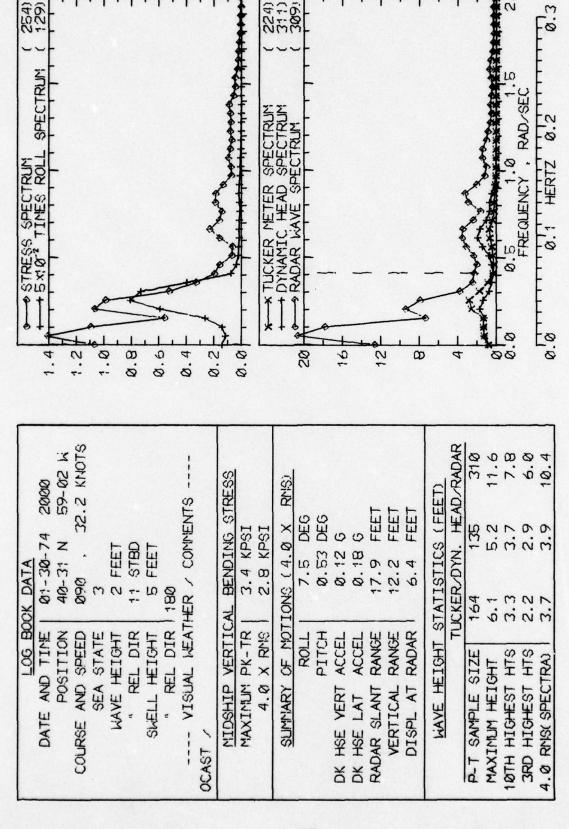
28

SPECTRUM

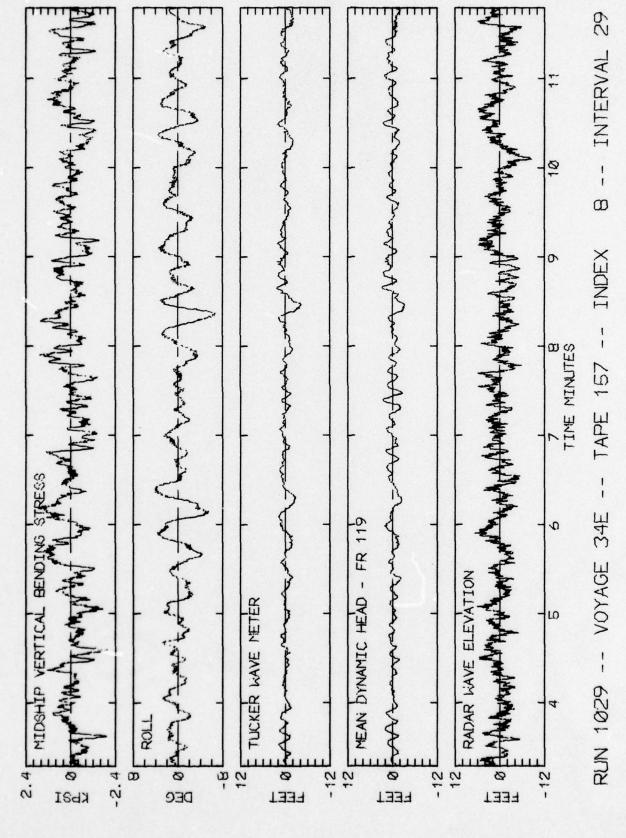
26 7 -- INTERVAL TAPE 157 -- INDEX 1 34E VOYAGE RUN 1026 --

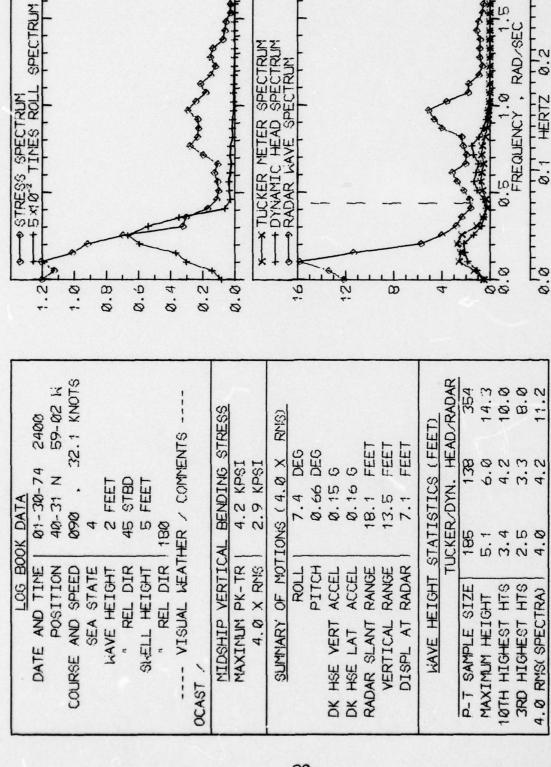
6.3



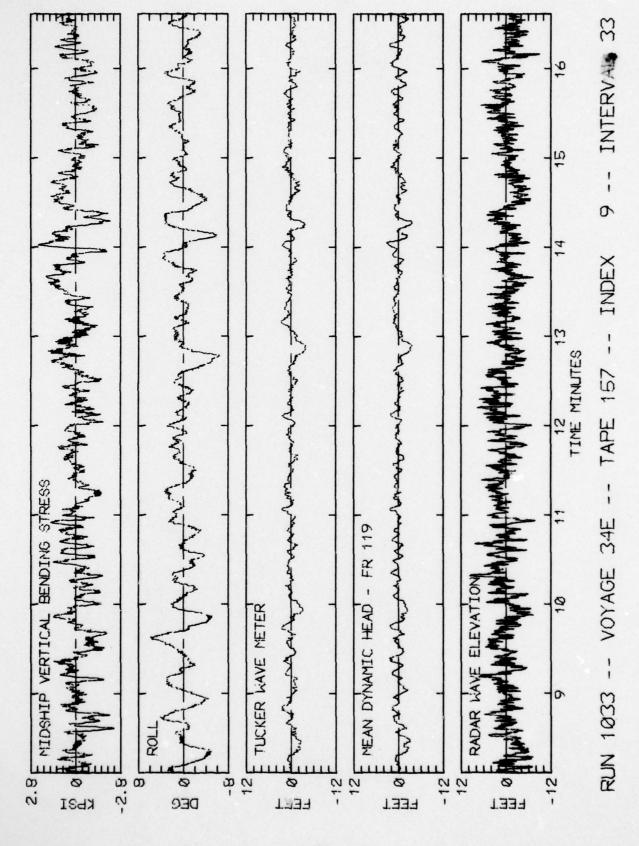


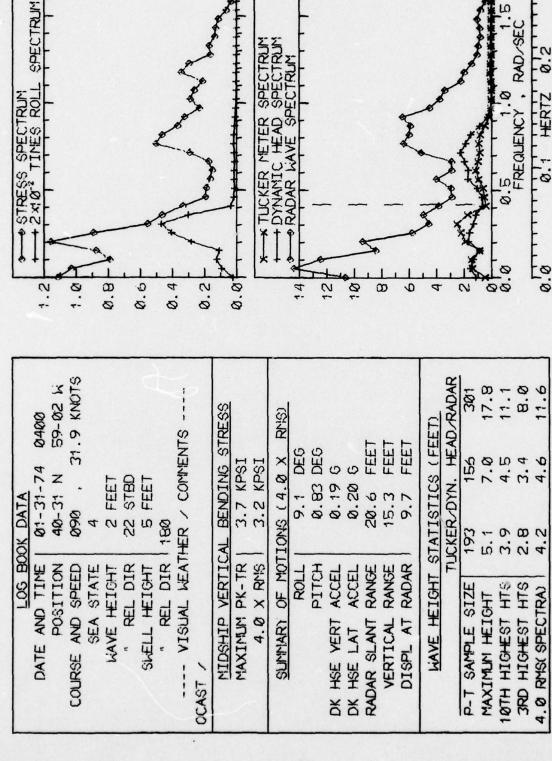
INTERVAL 29 1 80 INDEX 1 TAPE 157 RUN 1029 -- VOYAGE 34E



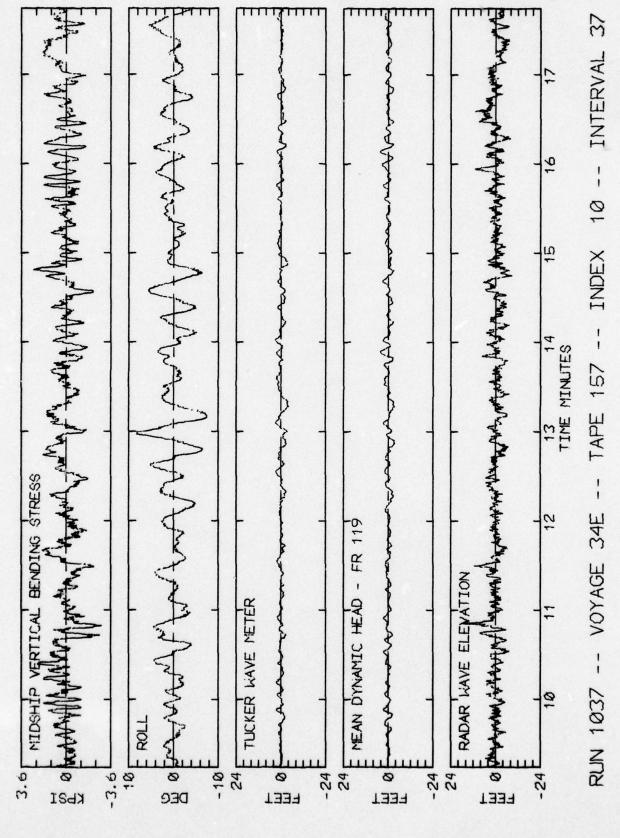


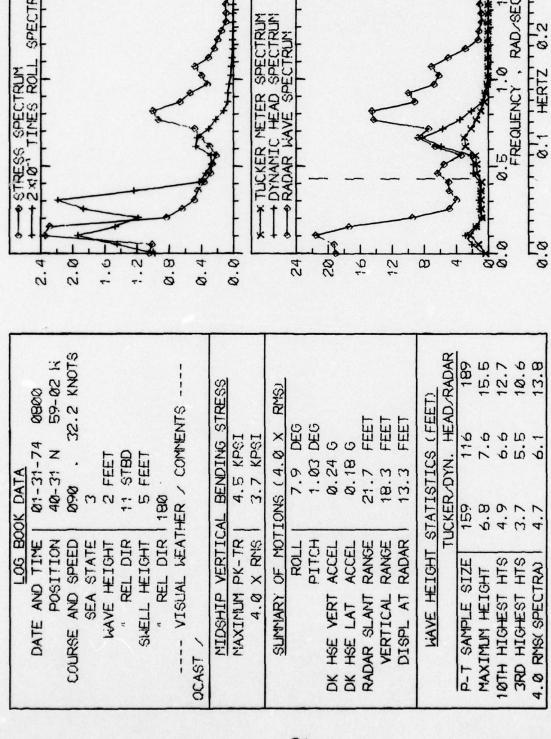
INTERVAL 33 -- 6 INDEX RUN 1033 -- VOYAGE 34E -- TAPE 157 --





RUN 1037 -- VOYAGE 34E -- TAPE 157 -- INDEX 10 -- INTERVAL



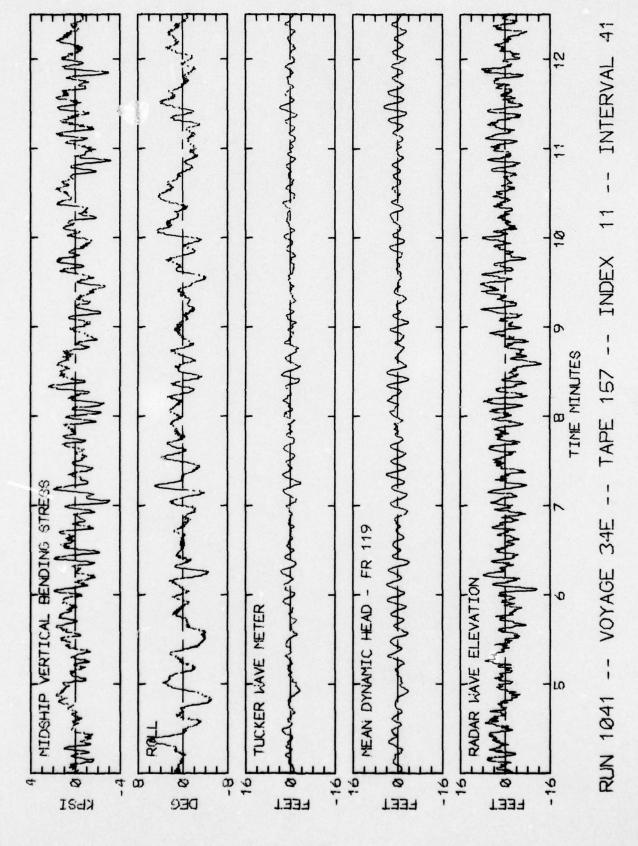


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SPECTRUN

7 INTERVAL INDEX 11 --1 157 TAPE VOYAGE 34E 1 RUN 1041

8.3



4 M N		8 9 8 8 8 9 8 8	0 00 0
	MIDSHIP VERTICAL BENDING STRESS MAXIMUM PK-TR 7.4 KPSI 4.0 X RMS 5.3 KPSI	SUMMARY OF MOTIONS (4.0 X RMS) ROLL 9.2 DEG PITCH 1.64 DEG DK HSE VERT ACCEL 0.39 G DK HSE LAT ACCEL 0.22 G RADAR SLANT RANGE 30.2 FEET VERTICAL RANGE 28.3 FEET DISPL AT RADAR 21.0 FEET	MAVE HEIGHT STATISTICS (FEET)

SOUTH SPECTRUM (173)

THES ROLL SPECTRUM (173)

THES ROLL SPECTRUM (173)

THES ROLL SPECTRUM (173)

SOUTH SPECTRUM (173)

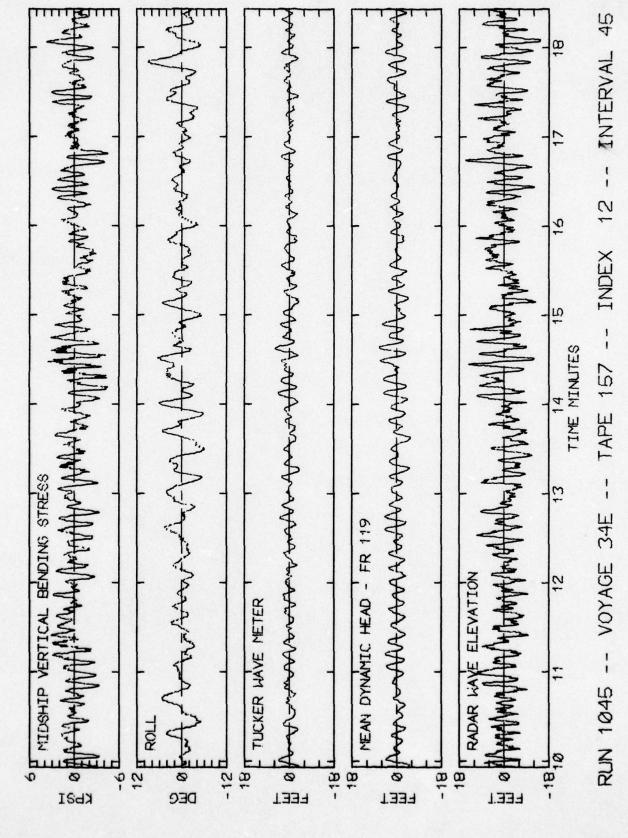
THE SPECTRUM (173)

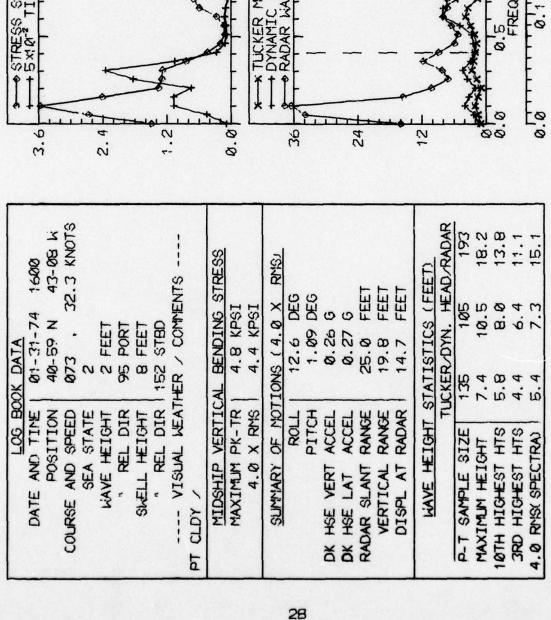
SOUTH SPECTRUM (173)

THE SPECTRUM (173)

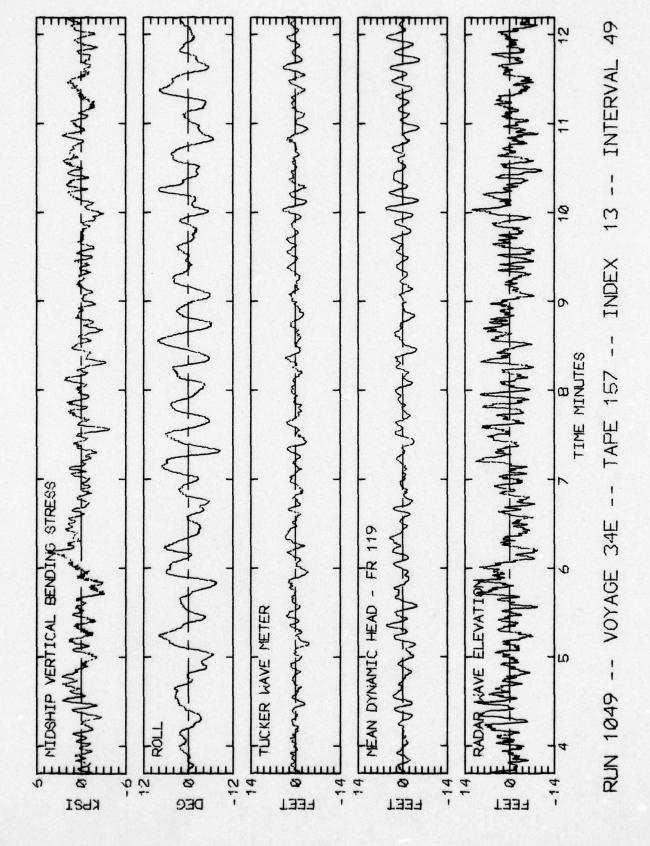
SOUTH SPECTRUM

RUN 1045 -- VOYAGE 34E -- TAPE 157 -- INDEX 12 -- INTERVAL 45





49 INTERVAL INDEX 13 --1 157 TAPE VOYAGE 34E RUN 1049 --

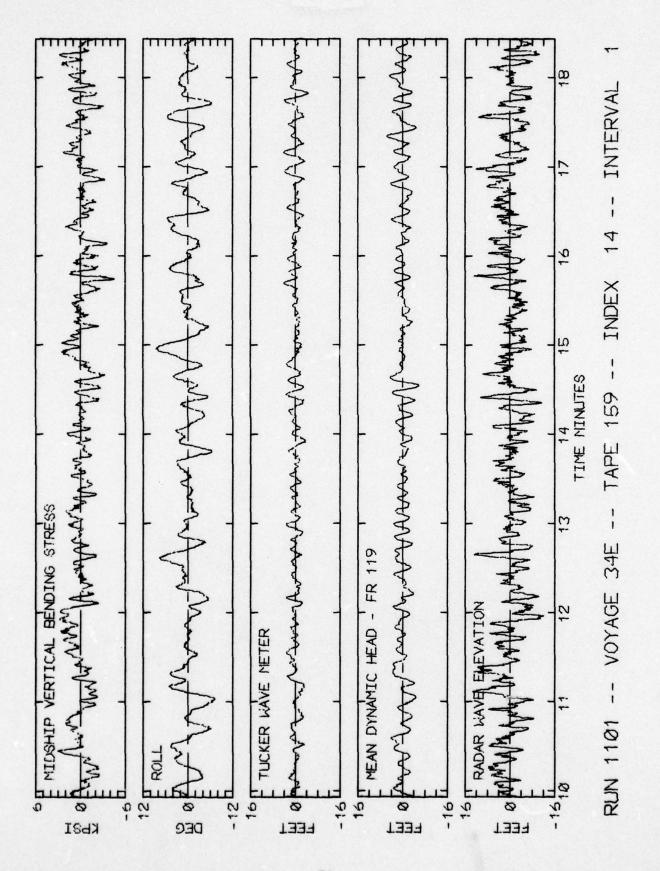


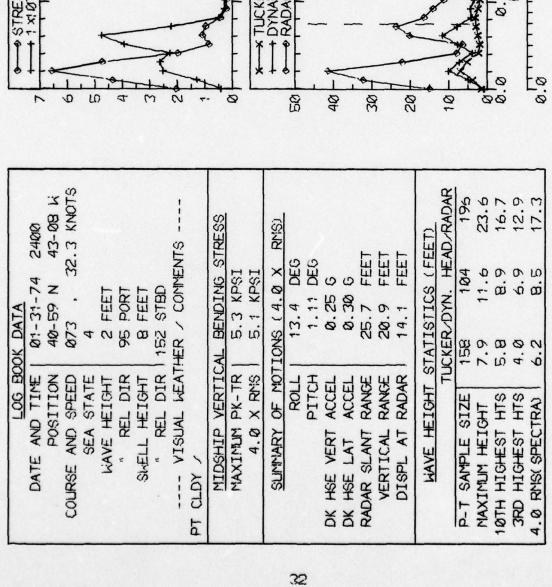
3 - STRESS SPECTRUM 3 - 1 x/0" TINES ROLL SPECTRUM 2 - 1 x/0" TINES ROLL SPECTRUM	28 PECTRUM 28 PECTRUM 29 RADAR MAYE SPECTRUM 20 16 16 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18	8 - 4 - 10 0 E FREQUENCY RAD/SEC
DATE AND TIME 81-31-74 2000 POSITION 40-59 N 43-08 W SEA STATE 2 FEET WAVE HEIGHT 50 PORT SIJELL HEIGHT B FEET REL DIR 50 PORT REL DIR 152 STBD VISUAL MEATHER / COMMENTS MAXIM PK-TR 1 7 7 KPST	X RNS OF MOTION ROLL PITCH ACCEL RANGE RADAR	TUCKER_DYN. HEAD_RADAR TUCKER_DYN. HEAD_RADAR 193 193 194 194 187 18

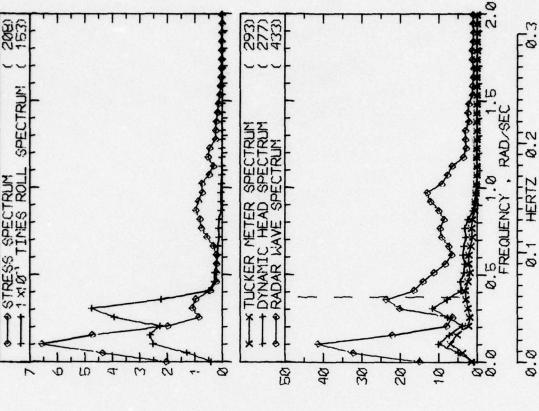
265)

SPECTRUM

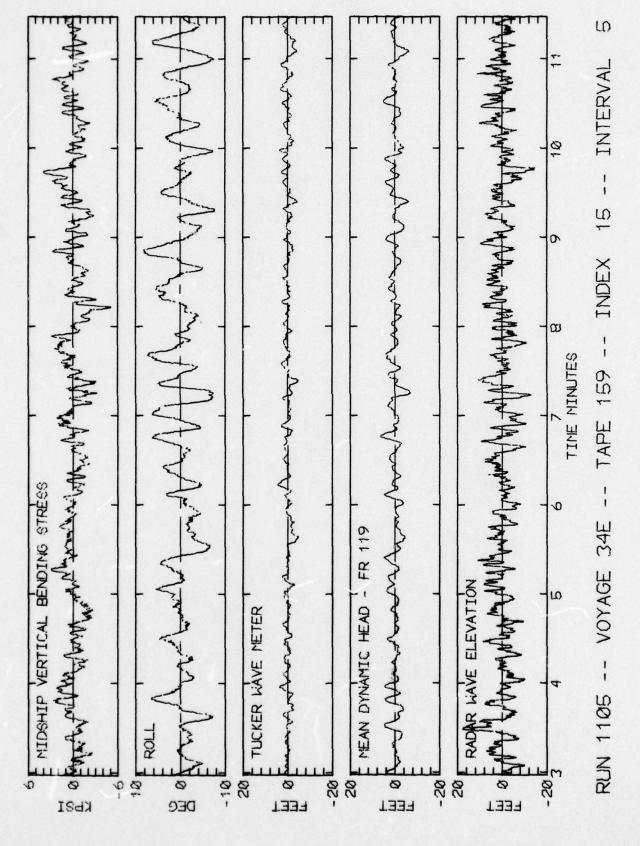
RUN 1101 -- VOYAGE 34E -- TAPE 159 -- INDEX 14 -- INTERVAL

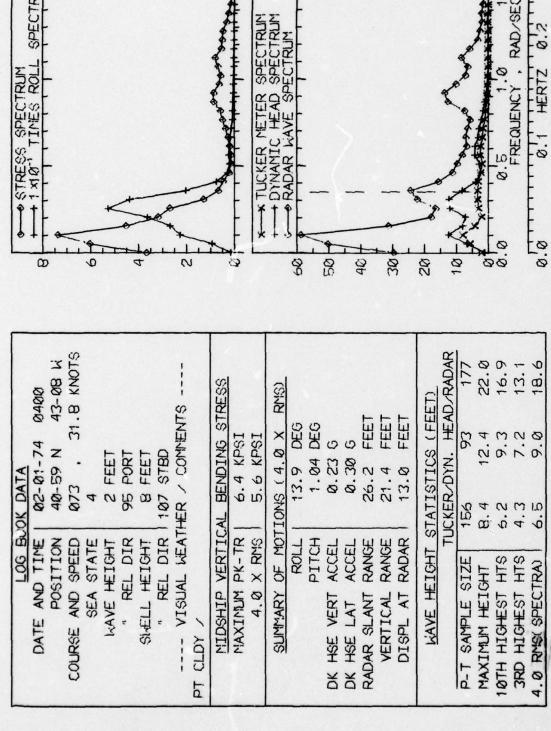






D INTERVAL 1 5 INDEX 1 159 TAPE RUN 1105 -- VOYAGE 34E

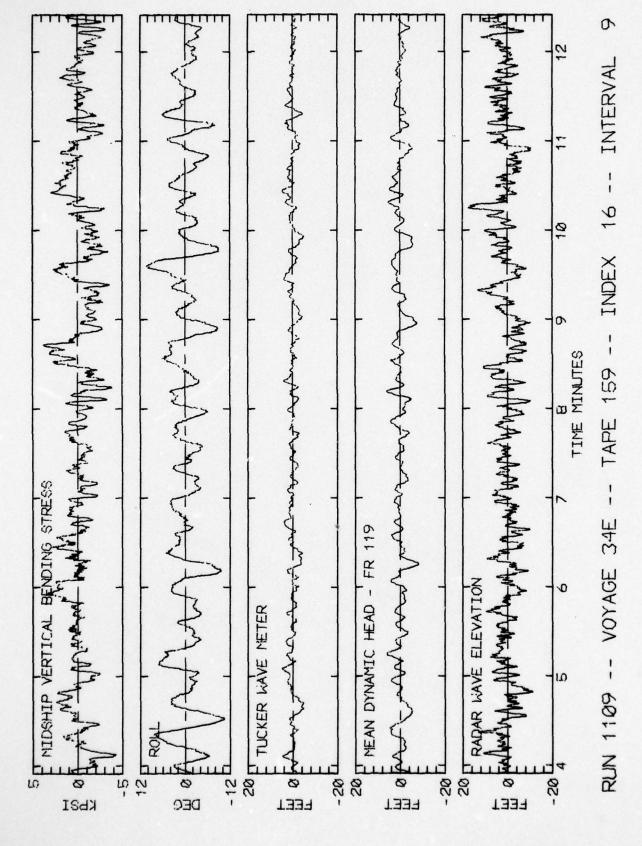


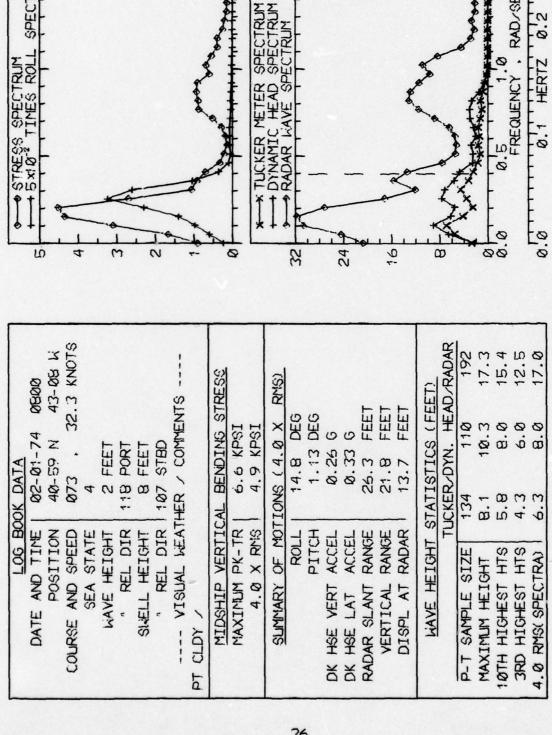


2033

SPECTRUN

0 INTERVAL INDEX 16 --TAPE 159 VOYAGE 34E RUN 1109 --





252

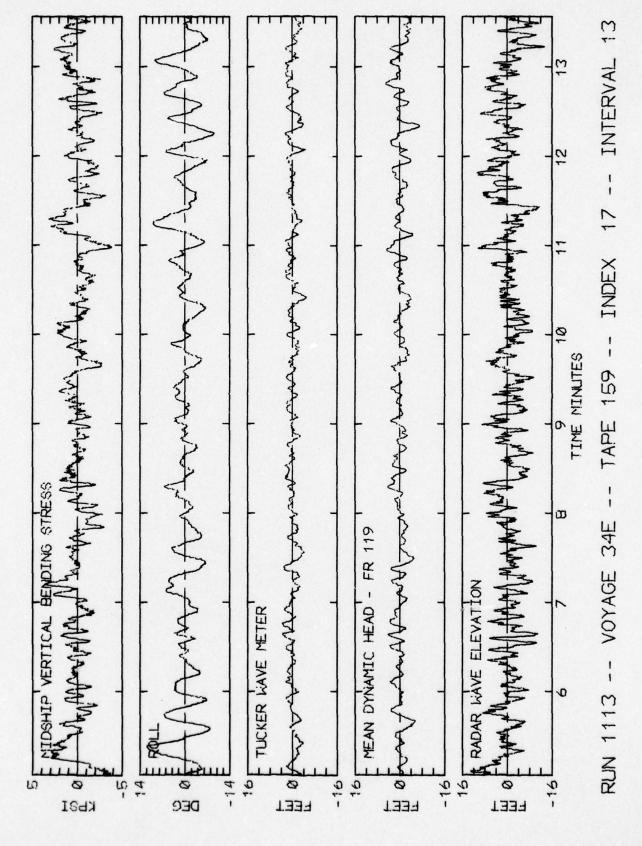
SPECTRUM

3 INTERVAL 17 --INDEX 1 159 TAPE 1 34E VOYAGE 1 RUN 1113

6.3

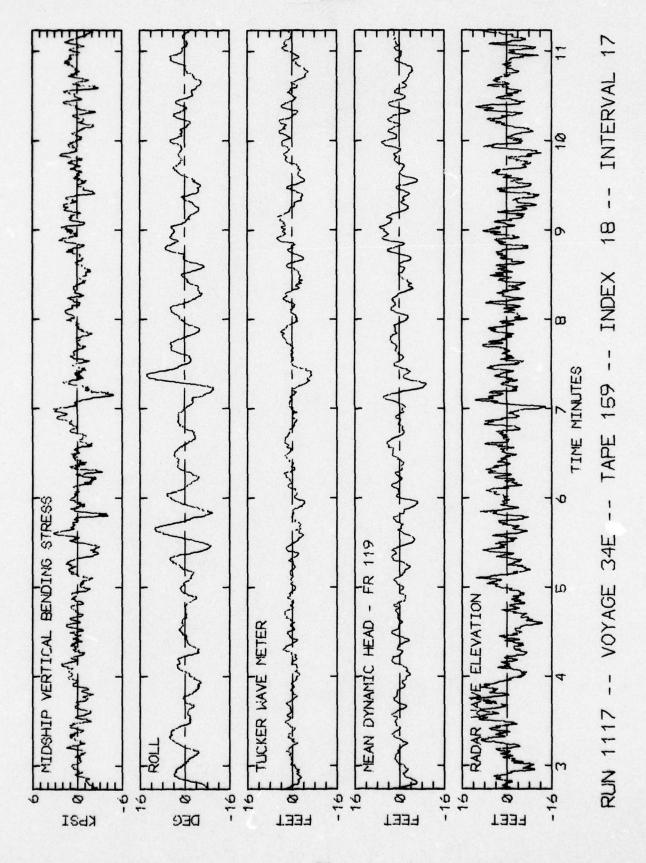
0.2

, RAD/SE

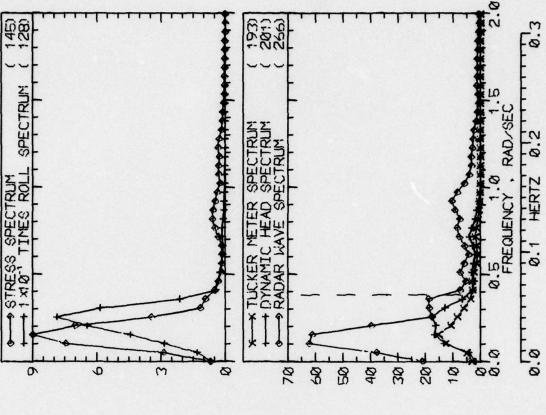


3.5 C STRESS SPECTRUN (260)	0.0 X TICKER NETER SPECTRUM (1841)	36 RADAR WAVE SPECTRUM (219)	0.0 0.5 1.0 1.5 2.0 FREQUENCY RAD/SEC 0.3
1 44484 1	PT CLDY / NIDSHIP VERTICAL BENDING STRESS NAXIMUM PK-TR 8.8 KPSI 4.0 X RMS 4.7 KPSI	SUMMARY OF MOTIONS (4.0 X RMS) ROLL 15.7 DEG PITCH 0.98 DEG DK HSE VERT ACCEL 0.24 G DK HSE LAT ACCEL 0.35 G RADAR SLANT RANGE 26.9 FEET VERTICAL RANGE 28.7 FEET DISPL AT RADAR 13.2 FEET	P-T SAMPLE SIZE 116 73 173 MAXIMUM HEIGHT 9.3 15.2 22.1 10TH HIGHEST HTS 7.5 10.7 17.6 3RD HIGHEST HTS 5.3 8.2 13.4 4.0 RNS(SPECTRA) 8.5 9.9 17.7

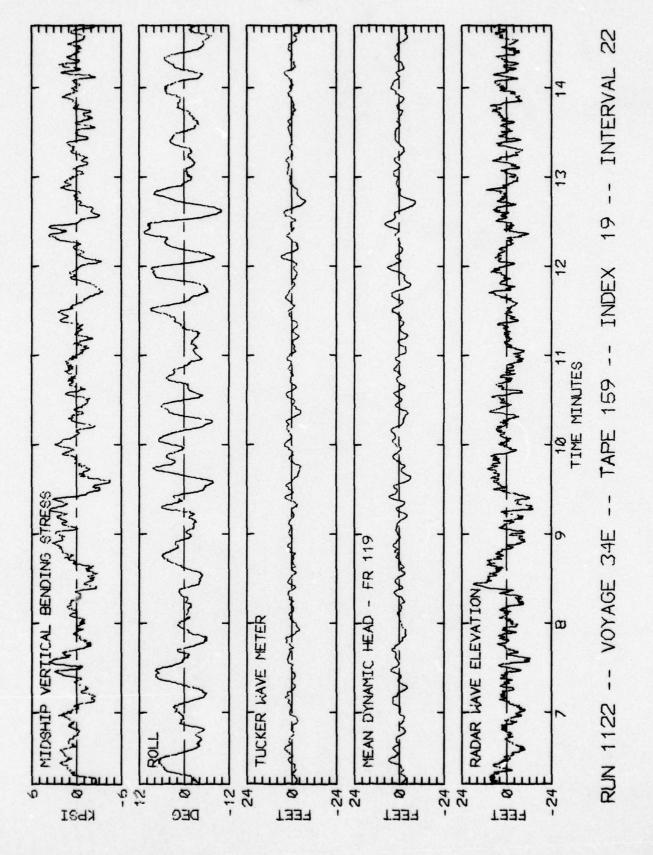
RUN 1117 -- VOYAGE 34E -- TAPE 159 -- INDEX 18 -- INTERVAL 17



STRESS STATES ST	SE S	20 10 0.0 0.0 0.5 FREQUE
DATE AND TINE 02-01-74 1600 POSITION 44-27 N 27-18 K 072 32.4 KNOTS SEA STATE 7 KAVE HEIGHT 4 FEET REL DIR 63 STBD VISUAL KEATHER / COMMENTS	MIDSHIP VERTICAL BENDING STRESS NAXINUM PK-TR 7.3 KPSI 4.0 X RMS 5.7 KPSI SUMNARY OF MOTIONS (4.0 X RMS) ROLL 16.5 DEG PITCH 0.95 DEG DK HSE VERT ACCEL 0.23 G DK HSE LAT ACCEL 0.23 G DK HSE LAT ACCEL 0.24 G RADAR SLANT RANGE 27.0 FEET VERTICAL RANGE 22.0 FEET DISPLAT RADAR 12.6 FEET	SIZE 105 SHT 11.6 HTS 8.5 HTS 8.5 HTS 8.5
	40	



RUN 1122 -- VOYAGE 34E -- TAPE 159 -- INDEX 19 -- INTERVAL 22



7 STRESS SPECTRUM THE STOLL SPECTR	19		46			2 + + 2	T.	Bearing the state of the state	* X THEKER NETER SPECTRIM	18	60 THE THE SPECIALITY		201			900	***	2007	***	是 · · · · · · · · · · · · · · · · · · ·		8.8 8.5 1.8	FREQUENCY , RAD/SEC	
-74	COURSE AND SPEED 072 , 32.3 KNOTS	SEA STATE 7	EL DIR 117	SWELL HEIGHT 6 FEET	" REL DIR 63 STBD	PT CLDY /	MIDSHIP VERTICAL BENDING STRESS	MAXIMUM PK-TR 6.4 KPSI	X RMS	SUMNARY OF MOTIONS (4.0 X RNS)	ROLL 18.0 DEG	PITCH 1.04 DEG	DK HSE VERT ACCEL 0.24 G	DK HSE LAT ACCEL 0.39 G	RADAR SLANT RANGE 29.3 FEET	VERTICAL RANGE 22.6 FEET	DISPL AT RADAR 15.0 FEET		TUCKER/DYN. HEAD/RADAR	P-T SAMPLE SIZE 116 94 176	MAXIMUM HEIGHT 8.8 17.6 25.7	10TH HIGHEST HTS 7.7 11.1 18.1	3RD HIGHEST HTS 6.2 8.6 14.7	O OL C AL C O CAUTOTO A

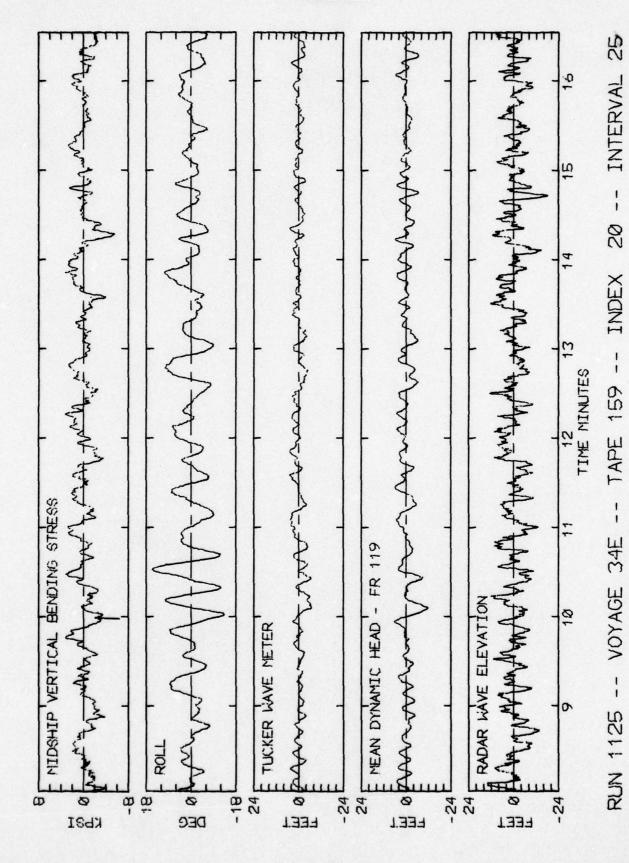
The state of the s

1741

SPECTRUM

77 9.2

RUN 1125 -- VOYAGE 34E -- TAPE 159 -- INDEX 20 -- INTERVAL 25



2400 TINES SPECTRUM	B Ki		<u>*</u>	/ 1 7	n i	2	\$		A A A A A A A A A A A A A A A A A A A	*** TUCKER METER SPE	VAMIC HEAD	70 TAUAK WAVE SPEC		86	20 / / 205		40	30-	20 - 20 -	HEAD/RADAR IN ATT	140 100		22.5 0.0 0.5 1.0	17.1 FREQUENCY .	6.0
DATE AND TIME 1 02-01-74 24	44-27 N	STATE 7	WE HEIGHT 4	SHELDIR 175 STBD	REL DIR 63		PT CLDY /	MIDSHIP VERTICAL BENDING STRESS	PK-TR	4.0 X RNS 5.5 KPSI	SUMMARY OF MOTIONS (4.8 X R	ROLL 18.4 DEG	PITCH 1.04 DEG	DK HSE VERT ACCEL 0.26 G	DK HSE LAT ACCEL 0.41 G	T RANGE	VERTICAL RANGE 24.9 FEET	DISPL AT RADAR 18.8 FEET		TUCKER/DYN. HEAD	P-T SAMPLE SIZE 78 79	MAXIMUM HEIGHT 13.5 16.8	10TH HIGHEST HTS 12.3 13.9	3RD HIGHEST HTS 9.8 11.4	4.0 RMS(SPECTRA) 12.1 13.7

215

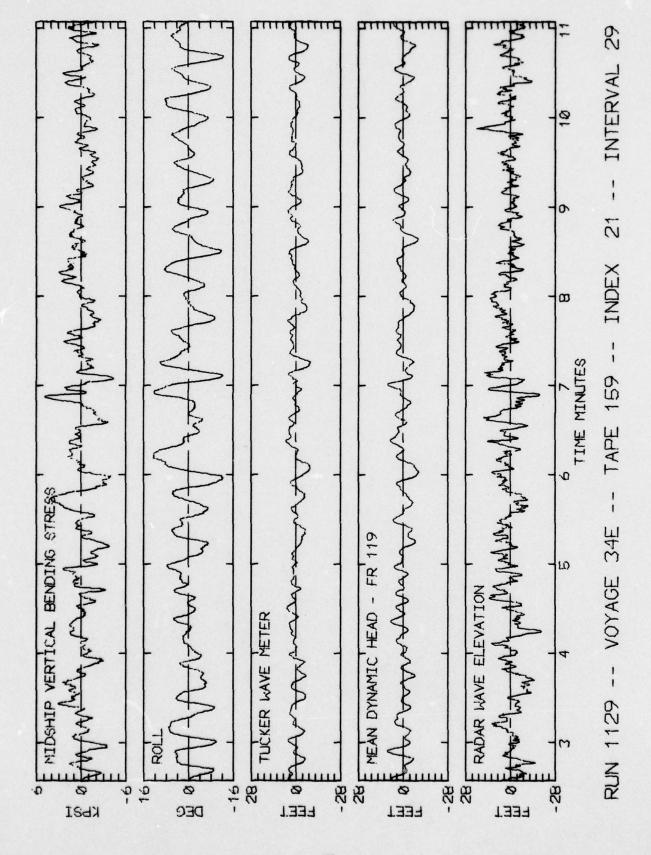
SPECTRUM

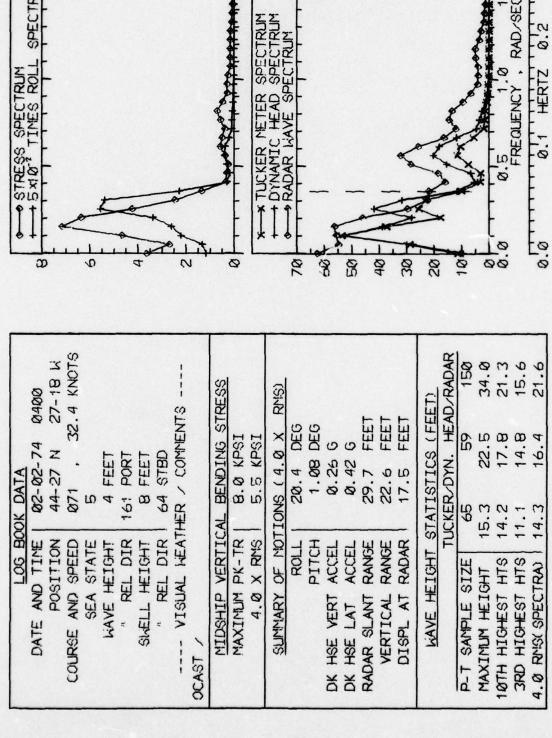
'S 1.0 1.5 FREQUENCY , RAD/SEC 011 HERTZ 0.2

INDEX 21 -- INTERVAL 29

TAPE 159 --

RUN 1129 -- VOYAGE 34E

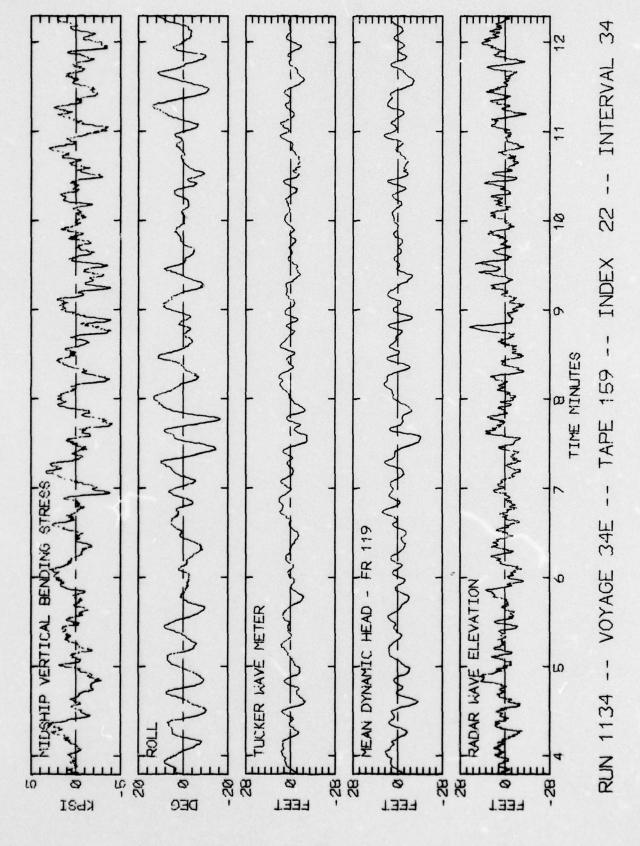


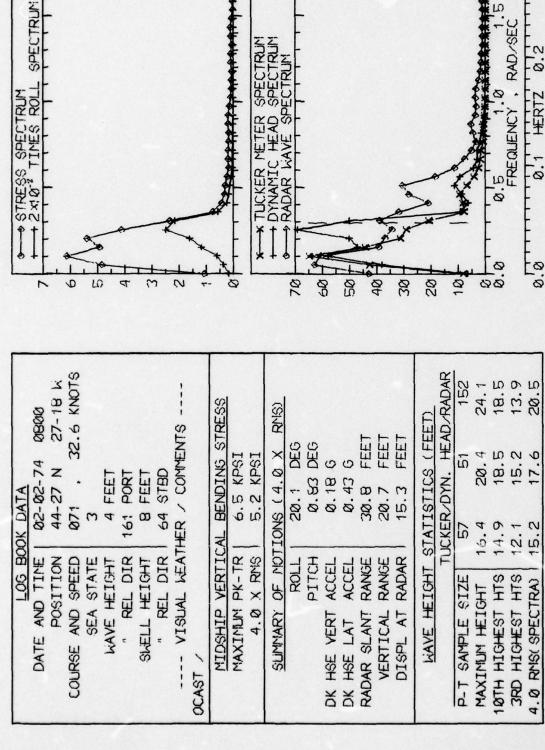


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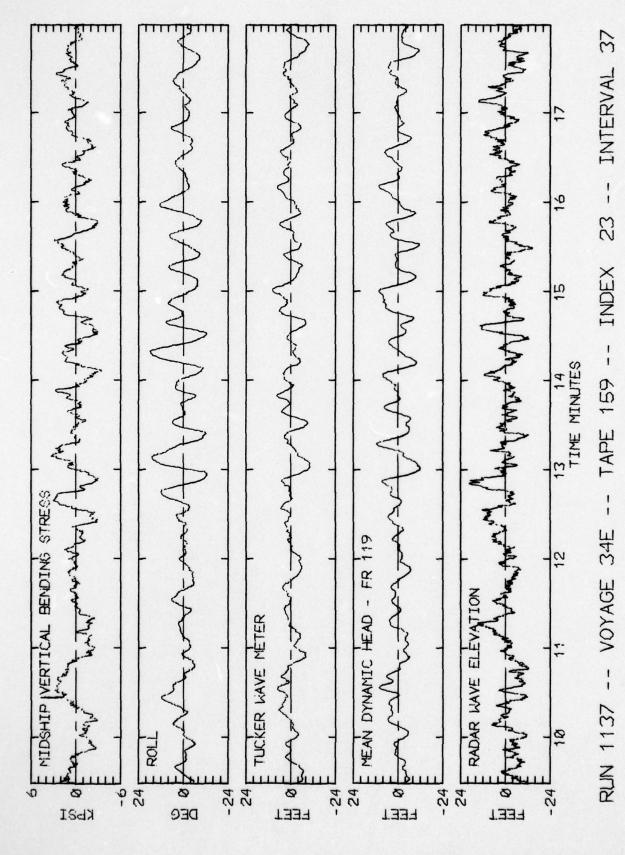
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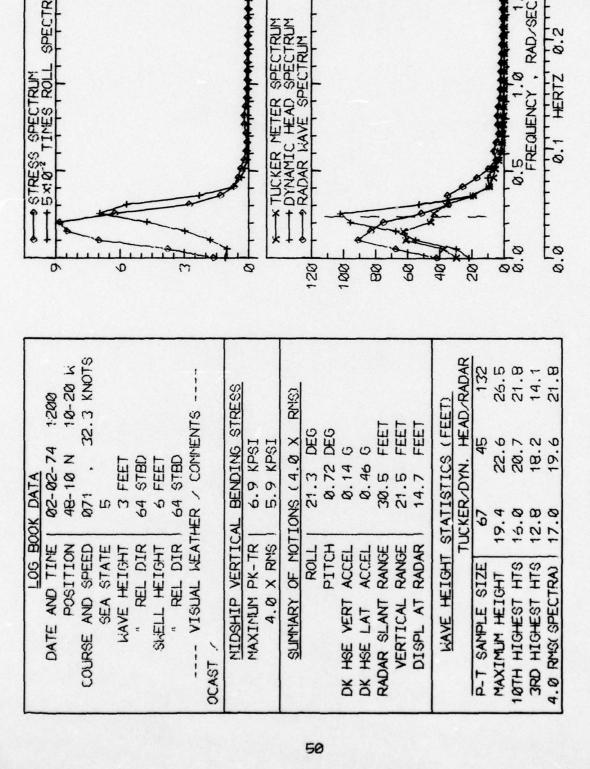
3.4 RUN 1134 -- VOYAGE 34E -- TAPE 159 -- INDEX 22 -- INTERVAL





37 INTERVAL 23 --VOYAGE 34E -- TAPE 159 -- INDEX RUN 1137 --



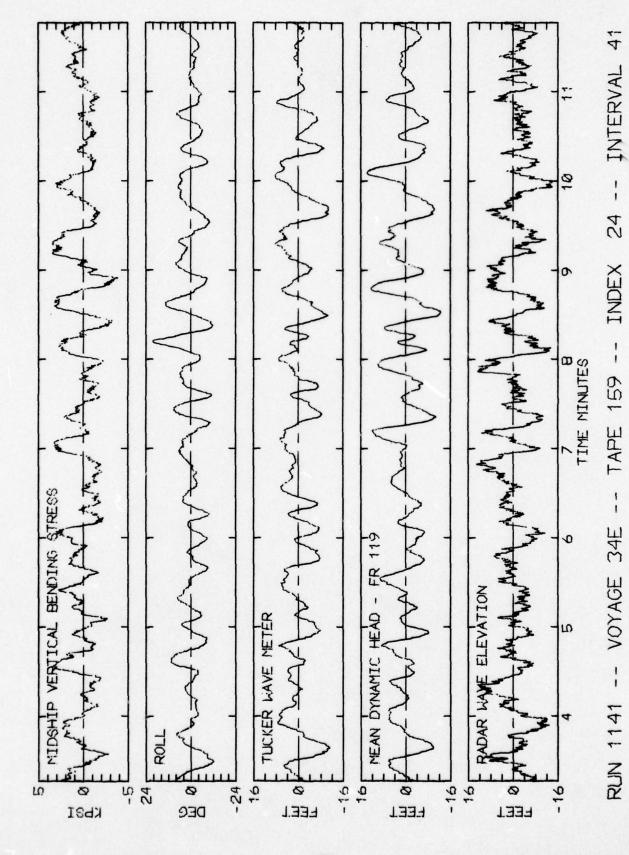


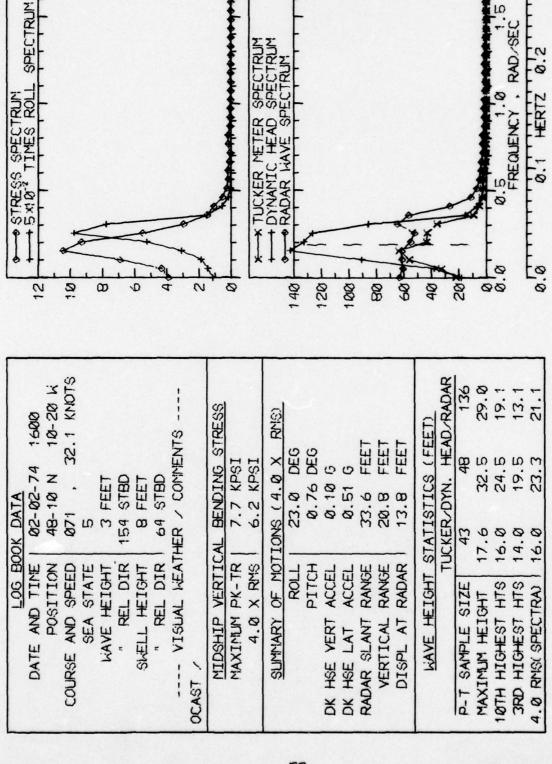
33

SPECTRUM

4 INTERVAL 1 77 INDEX 1 159 TAPE 1 RUN 1141 -- VOYAGE 34E

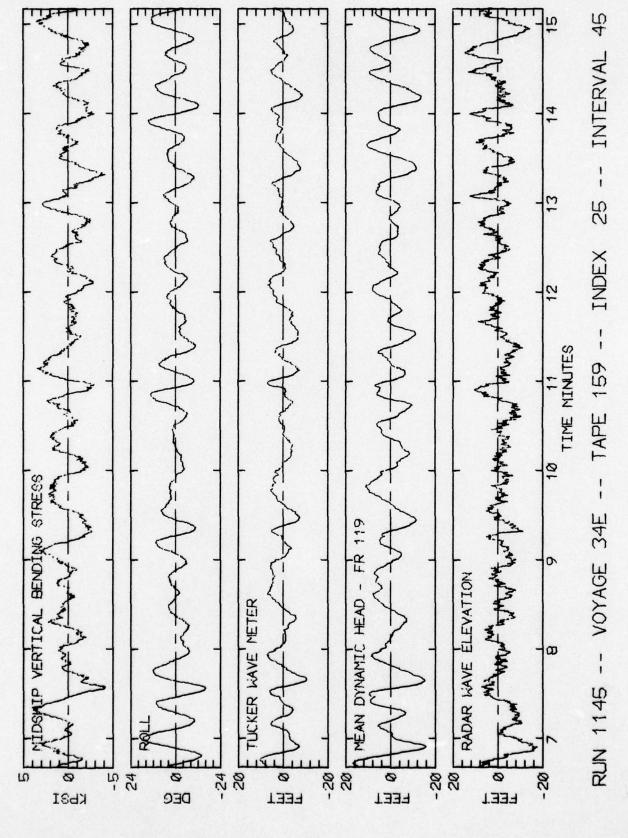
6.3

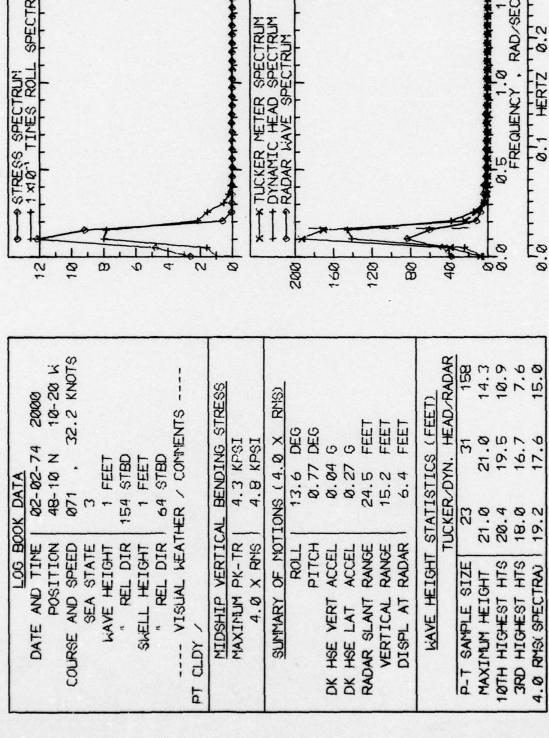




360

45 INTERVAL 25 --INDEX 159 --TAPE RUN 1145 -- VOYAGE 34E





SPECTRUM

40 INTERVAL 26 --TAPE 159 -- INDEX VOYAGE 34E RUN 1149 --

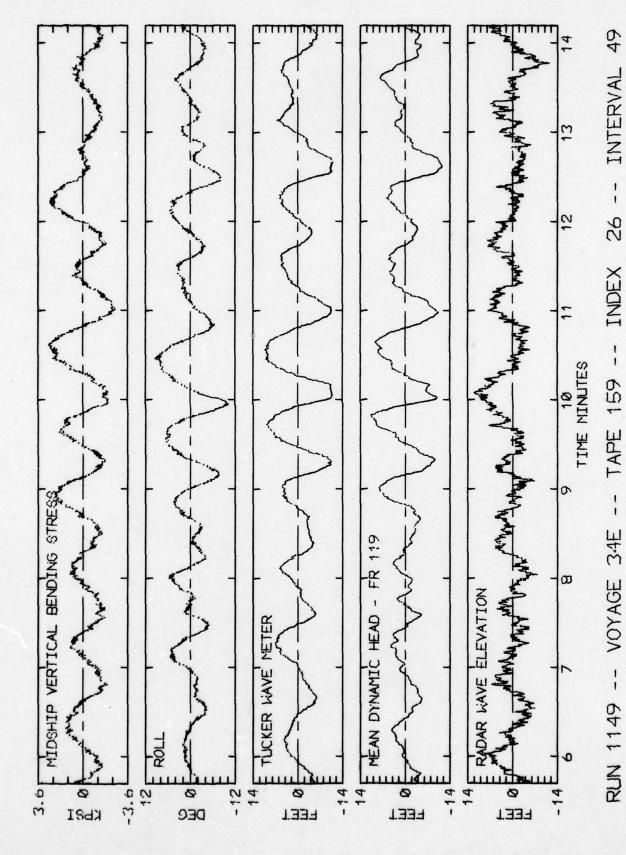


TABLE IIa

SUMMARY OF TMR LOG-BOOK DATA CORRESPONDING TO INTERVALS SELECTED FOR WAVE METER DATA REDUCTION (PAGE 1 OF 2)

SEA LAND MC LEAN : 1973-1974 WINTER SEASON : VOYAGE 34 WEST

(GMT) 0400 1200 0400 0400 0400 1200 1200 1200	(GMT) 0400 1200 0400 0400 0400 1200 1200 1600 0400 0800 0800	4 0000000000444444	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	LGNGITUDE 08-51 W 08-51 W 08-51 W 08-51 W 08-51 W 08-51 W 30-00 W 30-00 W 30-00 W 47-18 W 47-18 W 47-18 W 47-18 W 47-18 W 47-18 W 47-18 W 47-18 W		JR SE 12 2 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		SPEED 32.3 32.3 31.5 31.5 31.5 31.5 31.5 31.5 31.5 31	SPEED PROP KT. RPM 32.3 132.0 31.9 130.0 31.6 129.0 31.6 129.0 31.6 129.0 31.6 129.0 31.7 129.0 31.7 129.5 31.7 129.5 31.7 128.5 31.7 128.5 31.4 128.5 31.4 128.5 31.8 130.0 31.8 130.0
00000000000000000000000000000000000000			A 20000000000000444440000000000000000000	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX		LONGITUDE C 08-51 W 08-51 W 08-51 W 08-51 W 08-51 W 08-51 W 30-00 W 30-00 W 47-18 W 47-18 W 47-18 W 47-18 W 47-18 W 47-18 W	LONGITUDE COURSE 08-51 W 267 08-51 W 246 08-51 W 246 08-51 W 246 08-51 W 242 30-00 W 243 30-00 W 243 47-18 W 245	SPEED FR LUNGITUDE COURSE KT. R 08-51 W 267 31.9 130 08-51 W 246 30.8 127 08-51 W 246 31.3 128 08-51 W 246 31.6 129 08-51 W 242 31.6 129 30-00 W 243 31.7 129 30-00 W 243 31.7 129 47-18 W 243 31.4 128 47-18 W 245 31.3 128 47-18 W 245 31.3 128 47-18 W 245 31.8 130 47-18 W 245 31.8 130 47-18 W 245 31.9 128	SPEED FROP DRA LONGITUDE COURSE KT. RPM F 308 32.3 132.0 28. 08-51 W 267 31.9 130.0 29. 08-51 W 246 31.3 128.0 29. 08-51 W 246 31.4 129.0 29. 30-00 W 243 31.4 128.5 29. 30-00 W 243 31.4 128.5 29. 47-18 W 245 31.4 128.5 29.
# 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	000000000000000000000000000000000000000	*********		CGMT) LATI 0400 58- 22000 58- 2400 58- 0400 58- 1200 54- 1200 54- 1200 54- 1200 54- 1200 54- 0400 54- 04- 0400 54- 04- 04- 04- 04- 04- 04- 04- 04- 04- 0	TIME (GMT) LATITUDE 0400 1200 58-27 N 2400 58-27 N 0800 58-27 N 0400 54-00 N 1200 54-00 N 1200 54-00 N 0400 54-09 N 0400 48-09 N	TIME (GMT) LATITUDE LUNGITUDE 0400 1200 58-27 N 08-51 W 2400 58-27 N 08-51 W 0800 54-00 N 30-00 W 1200 54-00 N 30-00 W 1200 54-00 N 30-00 W 1200 48-09 N 47-18 W 0400 48-09 N 47-18 W 0800 48-09 N 47-18 W	TIME (GMT) LATITUDE LONGITUDE COURSE 0400 58-27 N 08-51 W 246 2400 58-27 N 08-51 W 246 0400 58-27 N 08-51 W 242 1200 58-27 N 08-51 W 242 1200 54-00 N 30-00 W 243 0400 48-09 N 47-18 W 245 0400 48-09 N 47-18 W 246 1200 48-09 N 47-18 W 246 1200 42-32 N 63-16 W 245	TIME (GMT) LATITUDE LUNGITUDE COURSE KT. R 0400 58-27 N 08-51 W 246 31.9 130 2400 58-27 N 08-51 W 246 31.9 128 0400 58-27 N 08-51 W 246 31.6 129 0400 58-27 N 08-51 W 246 31.6 129 0400 58-27 N 08-51 W 246 31.6 129 1200 54-00 N 30-00 W 241 31.6 129 1400 54-00 N 30-00 W 243 31.7 129 2400 54-00 N 30-00 W 243 31.3 128 0400 54-00 N 30-00 W 243 31.3 128 0400 54-00 N 47-18 W 243 31.4 128 1200 48-09 N 47-18 W 245 31.8 130 0400 48-09 N 47-18 W 245 31.8 130 0400 48-09 N 47-18 W 245 31.8 130	TIME (GMT) LATITUDE LONGITUDE COURSE KT. RPM F 60400 58-27 N 08-51 W 246 31.3 128.0 29. 2400 58-27 N 08-51 W 246 31.3 128.0 29. 2400 58-27 N 08-51 W 246 31.3 128.0 29. 2400 58-27 N 08-51 W 246 31.3 128.0 29. 2400 58-27 N 08-51 W 246 31.4 129.5 29. 1200 54-00 N 30-00 W 243 31.7 129.5 29. 1200 54-00 N 30-00 W 243 31.4 128.5 29. 1200 48-09 N 47-18 W 245 31.4 128.5 29. 1200 48-09 N 47-18 W 245 31.4 128.5 29. 0400 48-09 N 47-18 W 245 31.4 128.5 29. 0400 48-09 N 47-18 W 245 31.3 128.0 29. 0400 48-09 N 47-18 W 245 31.3 130.0 29. 0800 48-09 N 47-18 W 245 31.8 130.0 29. 1200 48-09 N 47-18 W 245 31.8 130.0 29. 1200 42-32 N 63-16 W 245 31.8 130.0 29.
MR TMR TMR DX INTU 0. 0. NO. NO. NO. NO. NO. NO. NO. NO. NO. NO		DATE 02-06-74 02-06-74 02-05-74 02-07-74 02-07-74 02-08-74 02-08-74 02-08-74 02-08-74		(GMT) 0400 1200 0400 0400 0400 1200 1200 1200	CGMT) LATITUDE 0400 1200 58-27 N 2400 58-27 N 0400 58-27 N 0400 58-27 N 0400 54-00 N 1200 54-00 N 1200 54-09 N 0400 54-32 N	TIME (GMT) LATITUDE LUNGITUDE 0400 1200 58-27 N 08-51 W 2400 58-27 N 08-51 W 0800 54-00 N 30-00 W 1200 54-00 N 30-00 W 1200 54-00 N 30-00 W 1200 48-09 N 47-18 W 0400 48-09 N 47-18 W 0800 48-09 N 47-18 W	TIME (GMT) LATITUDE LUNGITUDE COURSE 0400 58-27 N 08-51 W 246 2400 58-27 N 08-51 W 246 0400 58-27 N 08-51 W 246 0400 58-27 N 08-51 W 242 1200 54-00 N 30-00 W 243 1400 54-00 N 30-00 W 243 1200 54-00 N 30-00 W 243 1200 54-00 N 30-00 W 243 1200 48-09 N 47-18 W 245 0400 48-09 N 47-18 W 245 1200 48-09 N 47-18 W 245 1200 48-09 N 47-18 W 246 1200 42-32 N 63-16 W 245	TIME (GMT) LATITUDE LUNGITUDE COURSE KT. R 0400 58-27 N 08-51 W 246 31.9 130 2400 58-27 N 08-51 W 246 31.9 128 0400 58-27 N 08-51 W 246 31.6 129 0400 58-27 N 08-51 W 246 31.6 129 0400 58-27 N 08-51 W 246 31.6 129 1200 54-00 N 30-00 W 241 31.6 129 1400 54-00 N 30-00 W 243 31.7 129 2400 54-00 N 30-00 W 243 31.3 128 0400 54-00 N 30-00 W 243 31.3 128 0400 54-00 N 47-18 W 243 31.4 128 1200 48-09 N 47-18 W 245 31.8 130 0400 48-09 N 47-18 W 245 31.8 130 0400 48-09 N 47-18 W 245 31.8 130	TIME (GMT) LATITUDE LUNGITUDE COURSE KT. RPM F 60400 58-27 N 08-51 W 246 31.3 128.0 29. 2400 58-27 N 08-51 W 246 31.4 129.0 29. 2400 58-27 N 08-51 W 246 31.5 129.0 29. 2400 58-27 N 08-51 W 246 31.6 129.0 29. 2400 58-27 N 08-51 W 242 31.6 129.0 29. 1200 54-00 N 30-00 W 241 31.6 129.0 29. 1200 54-00 N 30-00 W 243 31.3 128.5 29. 1200 48-09 N 47-18 W 245 31.4 128.5 29. 1200 48-09 N 47-18 W 245 31.4 128.5 29. 2400 48-09 N 47-18 W 245 31.8 130.0 29. 2400 48-09 N 47-18 W 245 31.8 130.0 29. 2400 48-09 N 47-18 W 245 31.8 130.0 29. 2400 48-09 N 47-18 W 245 31.8 130.0 29. 2400 48-09 N 47-18 W 245 31.8 130.0 29. 2400 48-09 N 47-18 W 245 31.8 130.0 29. 2400 48-09 N 47-18 W 245 31.8 130.0 29.

TABLE 11b

SUMMARY OF TMR LOG-BOOK DATA CORRESPONDING TO

		INTER	RUALS (SELECT	ED FOR	WAVE METER	INTERVALS SELECTED FOR WAVE METER DATA REDUCTION (PAGE 2 OF 2)
		SEA		MC LE	AN : 19	73-1974 W.	LAND MC LEAN : 1973-1974 WINTER SEASON : VOYAGE 34 WEST
RUN.	SEA STATE	<pre><rel wind=""> DIR/SPEED </rel></pre>	REL WAVE DIR	WAVE HT.	REL SWELL DIR	<-SWELL-> HT LENGTH FT. FT.	> + VISUAL WEATHER /TMR LOG-BOOK COMMENTS
1209	4	83P/15	83P	T			PT CLDY /
1217		1385/25	1388	S	1158	8 150	OCAST /HEAVY ROLL
1228		1365/35	1368	ID.	1368	8 150	PT CLDY /HEAVY ROLL
1230		156P/10	156P	4	1365	6 150	PT CLDY /RIDING EASY
1233	S	100P/20	100F	CI	1145	6 150	OCAST /
1237	9	118P/25	118P	N	1185	6 150	OCAST /
1241	2	106P/10	106P	M	1198	6 150	OCAST FOG RAIN /
1245	2	103P/10	103P	N	1228	6 200	OCAST /
1305	M	18P/10	18P	2	18F	6 200	PT CLDY /
1309	9	498/25	495	S	18F	8 150	HAIL RAIN SQUALLS /
1317	7	498/ 5	498	N	278	8 150	CLEAR FOG SNOW /
1321	4	475/15	478	0	258	15 200	OCAST SNOW /ICE FIELD ROLLING HIGH SWE
1329	•0	928/25	928	N	258		OCAST /
1333	S	755/20	758	N	305	5 150	DCAST /
1337	S	1598/20	1598	N	248		OCAST SNOW /
1341	4	1375/15	1378	2	258	3 200	OCAST SNOW /
1345	4	1378/15	1378	N	1608	2 300	PT CLDY /

TABLE IIC

COMPARISON OF TMR RESULTS FOR MIDSHIP VERTICAL BENDING STRESS WITH CORRESPONDING RAW DIGITIZATION RESULTS AT DAVIDSON LABORATORY

SEA LAND MC LEAN : 1973-1974 WINTER SEASON : UOYAGE 34 WEST

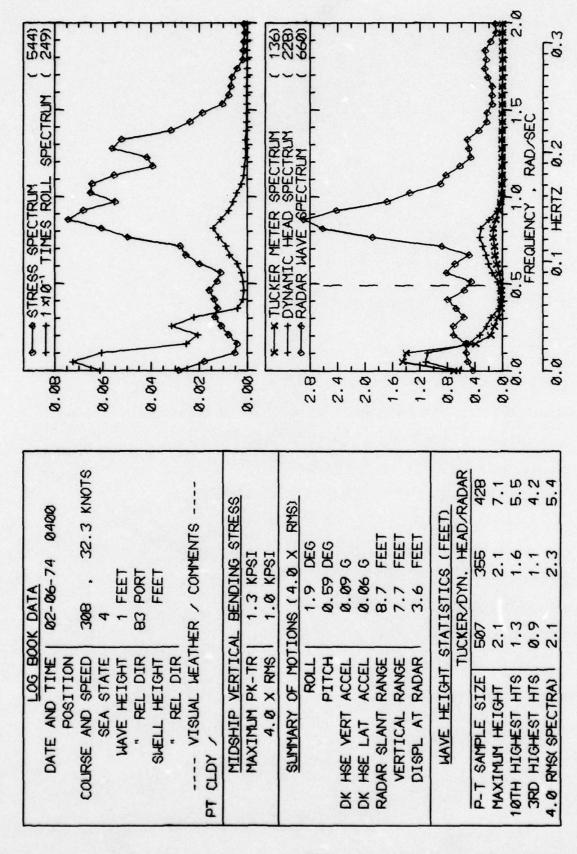
<s01< th=""><th>(9)</th><th>'</th><th>(3)</th><th></th><th></th><th>1.38</th><th>1.44</th><th>1.37</th><th>1.37</th><th>1,35</th><th>1.40</th><th>1.30</th><th>1.38</th><th>1.19</th><th>1.27</th><th>1.31</th><th>1.02</th><th>1.13</th><th>1.27</th><th>1.23</th><th>1.12</th><th>1.62</th></s01<>	(9)	'	(3)			1.38	1.44	1.37	1.37	1,35	1.40	1.30	1.38	1.19	1.27	1.31	1.02	1.13	1.27	1.23	1.12	1.62
MN RAT	(9)	,	(3+2)			1.38	1.09	1.21	1.09	1.21	1.21	1:11	1.14	0.93	0.91	1.07	1.02	0.93	0.95	1.05	1.12	1,13
corn	(2)	,	(4)			1.35	1.07	1.13	1.14	1.30	1.36	1.38	1.21	1.06	1.06	1.21	1.17	1.06	1.03	1.12	1.11	1.42
* *	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
.10N>	MEAN	STRESS	KPSI	(8)		3.53	0.01	0.28		1.55	2.05	0.28	1.89	90.0-	0.02	90.0	-0.04	0.18	0.21	0.18	-0.04	0.10
DIGITIZATION>* <column ratios=""></column>	(SAMPLE	RMS)	KPSI			0.73	5.21	5.95	5.49	4.73	5.19	4.16	4.98	6.15	5.99	4.70	3.53	3.68	4.54	2.66	1.22	1.22
->* <d.l.< th=""><th>RECORDED</th><th>EXTREMES</th><th>KPSI</th><th>(9)</th><th></th><th>1.83</th><th>14.62</th><th>15.15</th><th>12.58</th><th>11.69</th><th>11.69</th><th>8.76</th><th>12.34</th><th>17.51</th><th>18,31</th><th>12.14</th><th>8.49</th><th>6.39</th><th>13.32</th><th>99.9</th><th>3.20</th><th>2.99</th></d.l.<>	RECORDED	EXTREMES	KPSI	(9)		1.83	14.62	15.15	12.58	11.69	11.69	8.76	12.34	17.51	18,31	12.14	8.49	6.39	13.32	99.9	3.20	2.99
* *	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
>*<	MODE	STRES	KPSI	(2)		00.0	3.30	1.53	2.34	1.02	1.33	1.17	1.81	4.03	5.62	2.10	00.0	1.77	3.63	0.92	00.0	0.81
SE SE	F-T0-T	STRESS	KPSI	(4)		0.55	4.85	5.29	4.81	3.64	3.83	3.01	4.12	5.80	2.68	3.87	3.00	3.47	4.39	2.36	1.10	0.86
RESULTS	P-T0-T	STRESS	KPSI	(3)		1.32	10.16	11.02	9.21	8.66	8.34	6.72	8.97	14.77	14.43	9.26	8.34	8.31	10.46	5.41	2.87	1.84
NO.	1ST		A	(5)		0	44	23	19	S)	34	Ŋ	œ	09	57	43	0	45	44	N	0	N
NO.	* WAVE	INDUCED	CYCLES	Œ		177	142	140	145	125	82	16	137	157	154	138	117	198	181	197	192	139
* *			*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
	D.L.	RUN	NO.			1209	1217	1228	1230	1233	1237	1241	1245	1305	1309	1317	1321	1329	1333	1337	1341	1345
								-	0													

TABLE 11d

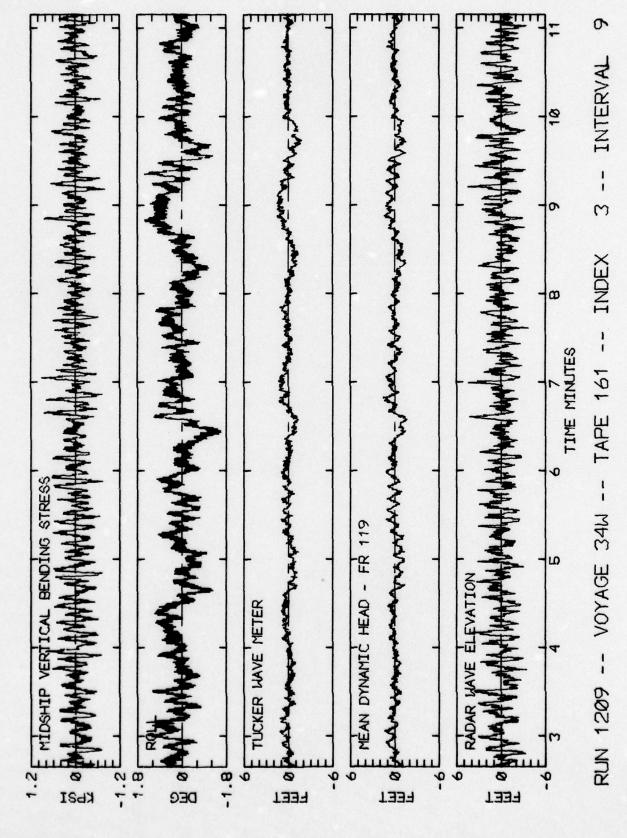
SUMMARY OF RAW DIGITIZATION RESULTS FOR RADAR RANGE ROLL, PITCH, DECK HOUSE ACCELERATIONS, AND TUCKER METER

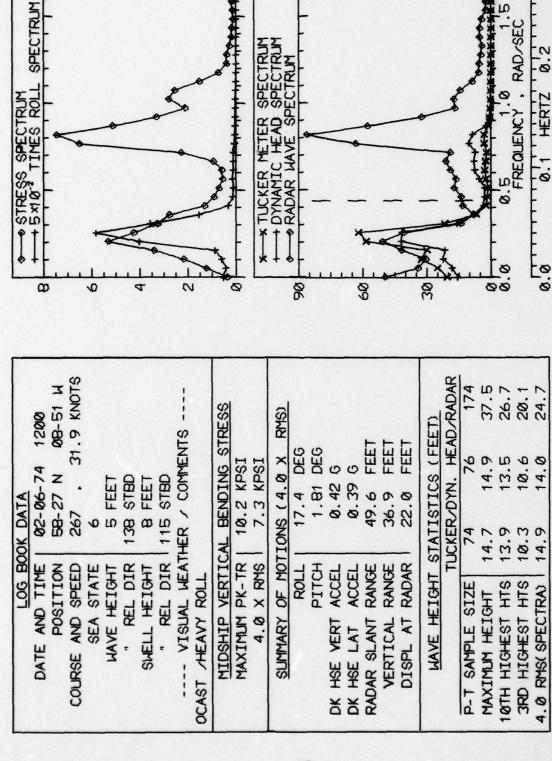
SEA LAND MC LEAN : 1973-1974 WINTER SEASON : UDYAGE 34 WEST

as-						
ORDE REME						444
TUCKER> 0 RECORDED S) EXTREMES T FT FT	10.	===		7.61	11.4.4	เมื่อผู้
4.0 (RMS) FT	2.15.19.	15.		9.	13.	4 m 0
ACCEL>< RECORDED EXTREMES (6) (6)	0.00	00.0	999	000	00.0	999
ACCI RECI EXTI (6)	0.0	0.3	000	000	0.1	0000
(RMS)	0.06	0.34	0.22	0.19	0.36	0.07
r ACCEL->< RECORDED EXTREMES						1000
∞ш~	146	000	000	0 0 0 0 0 0	0.0	0000
4.0 (RMS) (G)	0.09	0.35	0.19 0.18 0.27	0.50	0.15	0.23
	22.9	1.9	440	12.4	2.1	11.1
PITCH>< RECORDED EXTREMES DEG DEG	11.0	0.00	000	1.7 -	0.0	400
4.0 (RMS) DEG						00.79
ORDED ORDED REMES	-19.	-14.	1 8 8	-7. -9.	-16. -8.	44.4
ROLL - RECC EXTR	10.	0.00	9 0 0		77.	- 600
OULU	2.0	15.7	8 8 6	8.0 10.1 16.2	16.5	50.00
RADAR>< RECORDED 4.0 EXTREMES (RM)	-52.	-46.	-23. -19.	-44.	-25.	-16.
DAR RECO EXTR FT	59.	32.	\$ 55.	33.	31.	13.
< RA 4.0 (RMS) FT	500.	36.	31.	4 4 4 4 3	33.	12.
P.L. NO.	1209 1217 1228	1230	1237 1241 1245	1305 1309 1317	1321	1337 1341 1345
		59				



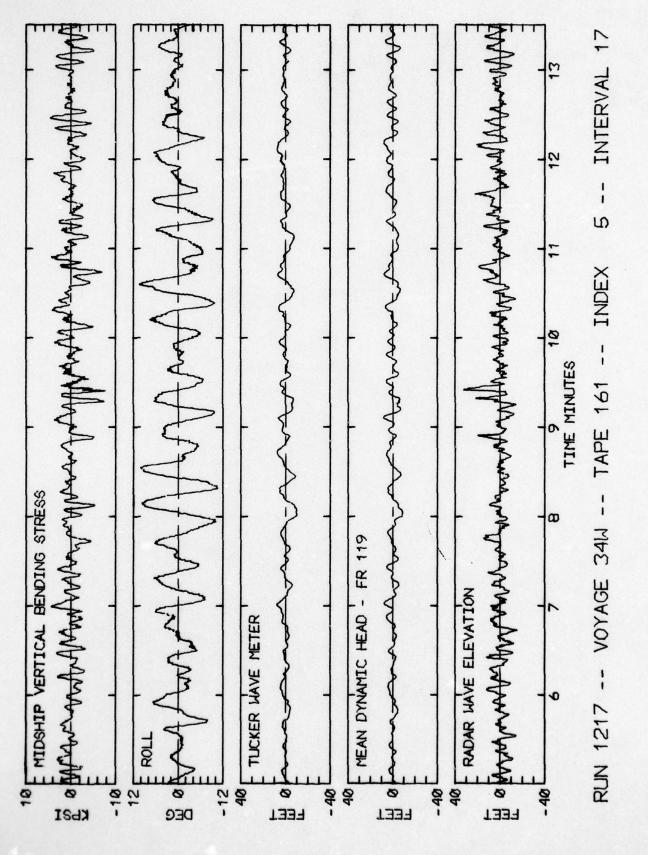
INTERVAL 3 --INDEX 1 **TAPE 161** RUN 1209 -- VOYAGE 34W --

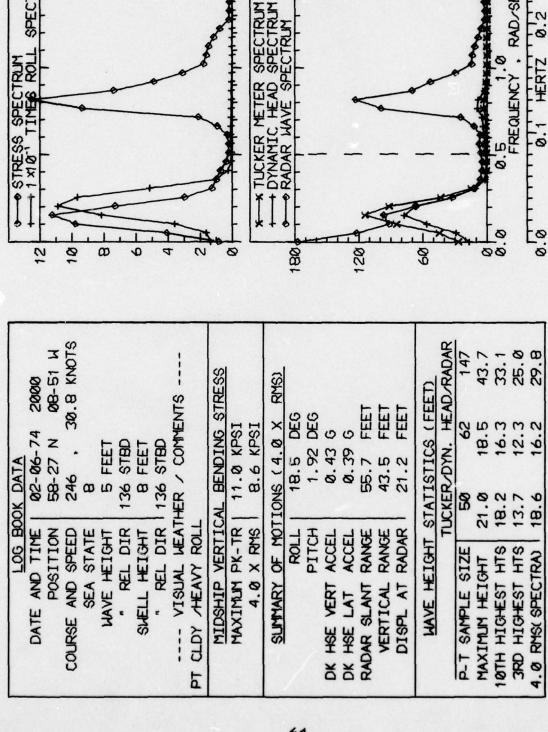




346)

INTERVAL 17 1 5 INDEX 1 **TAPE 161** 1 34M VOYAGE 1 RUN 1217





246)

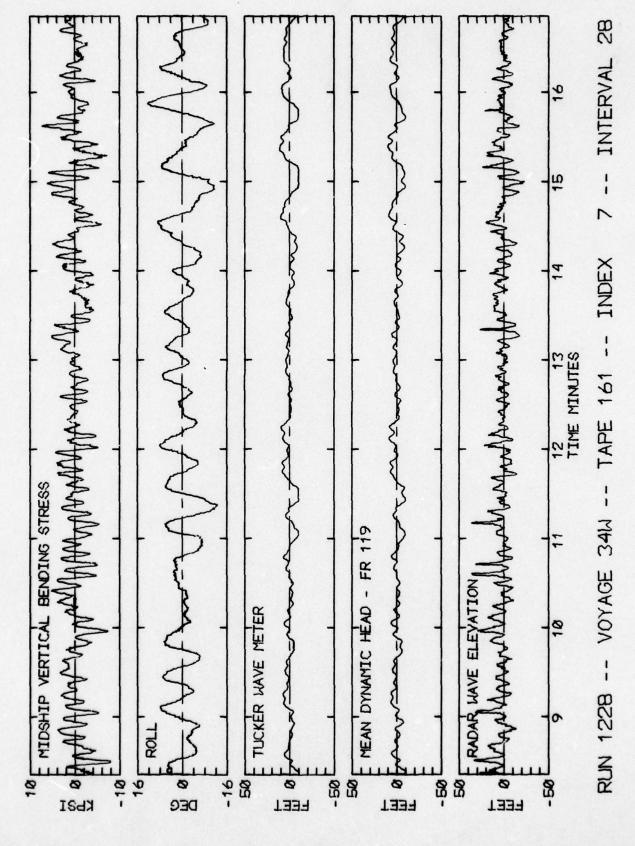
SPECTRUM

28 INTERVAL -- / INDEX 1 **TAPE 161** 1 34M VOYAGE 1 RUN 1228

6.3

0.2

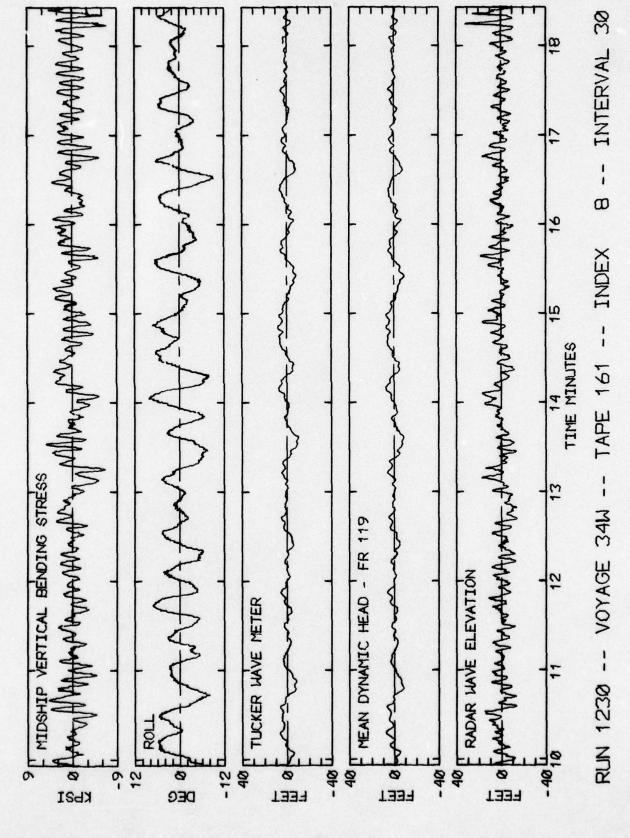
. RADISE

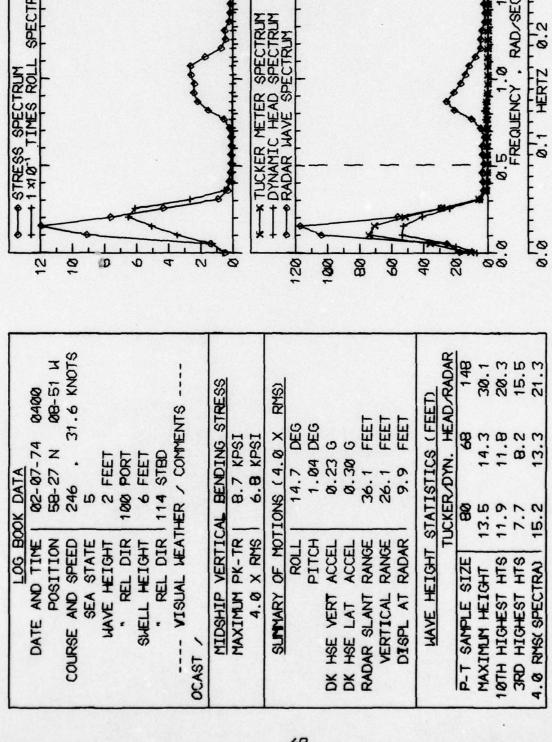


12 SPECTRI 18 SPECTRI 18 SPECTRI 18 SPECTRI 19 SPECTRI 10 SPE	SO THE SPECIAL	8.0 0.5 FREGLENCY
E AND TIME 02-06-74 2400 POSITION 58-27 N 08-51 W AND SPEED 246 , 31.3 KNOTS SEA STATE 3 AVE HEIGHT 4 FEET ELL HEIGHT 6 FEET REL DIR 136 STBD VISUAL WEATHER / COMMENTS	AL BENDING STRESS 9.2 KPSI 7.8 KPSI 10NS (4.0 X RMS) 15.6 DEG 1.61 DEG 0.35 G 0.35 G 0.35 G 33.2 FEET 15.6 FEET	MAVE HEIGHT STATISTICS (FEET) TUCKER_DYN. HEAD_RADAR AMPLE SIZE 62 65 157 UM HEIGHT 15.0 16.3 41.9 IGHEST HTS 14.0 13.4 25.1 IGHEST HTS 10.7 10.0 19.5 SK SPECTRAJ 14.6 13.4 22.9
DATE AND TIME POSITION COURSE AND SPEED SEA STATE WAVE HEIGHT " REL DIR SMELL HEIGHT " REL DIR " REATH	MIDSHIP VERTICAL BENDING STANDED TO BE THE LAT ACCEL BENDING (4.0 X RPSI SUMMARY OF MOTIONS (4.0 X ROLL 15.6 DE PORTICAL RANGE 33.2 FEEDISPL AT RADAR 15.6 FEEDI	P-T SAMPLE SIZE MAXIMUM HEIGHT 10TH HIGHEST HTS 3RD HIGHEST HTS 4.0 RMS(SPECTRA)
	66	

138 141 383 383 SPECTRUM

INTERVAL 30 1 œ RUN 1230 -- VOYAGE 34W -- TAPE 161 -- INDEX

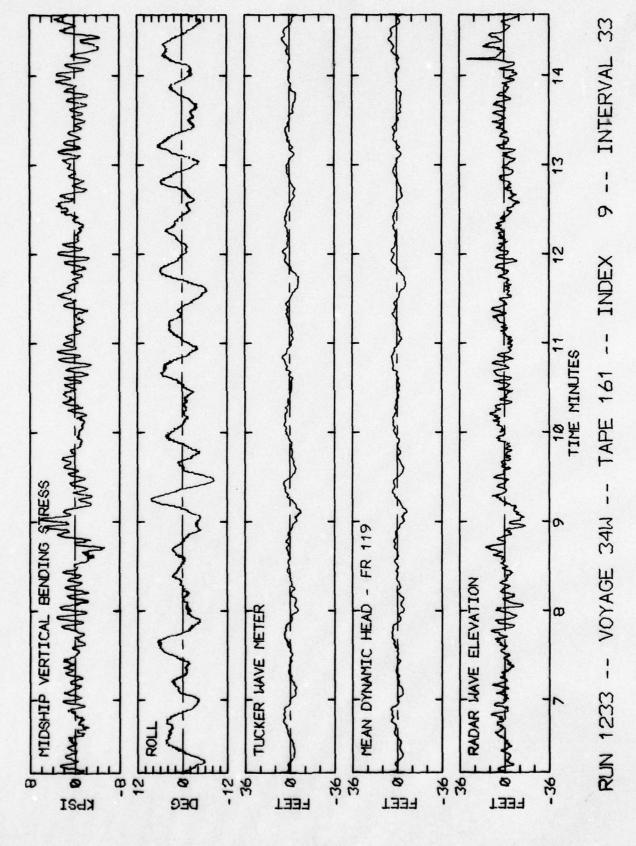


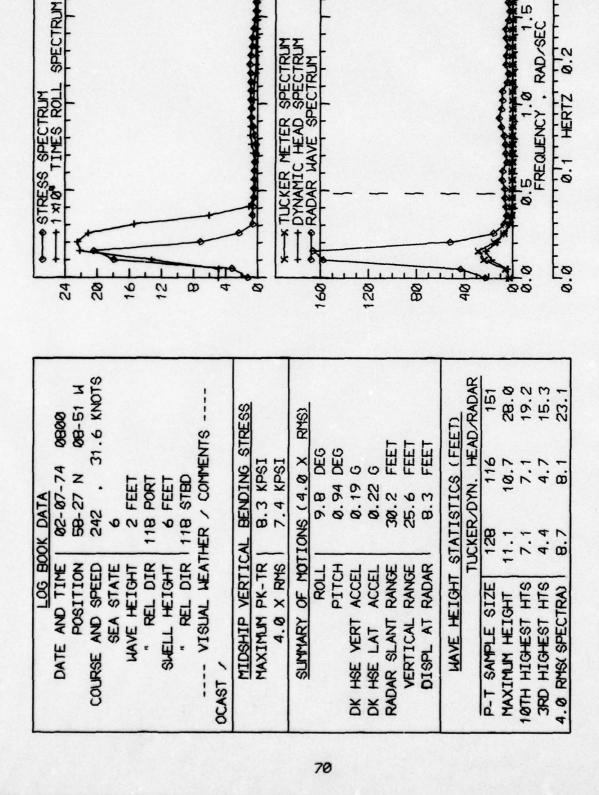


362

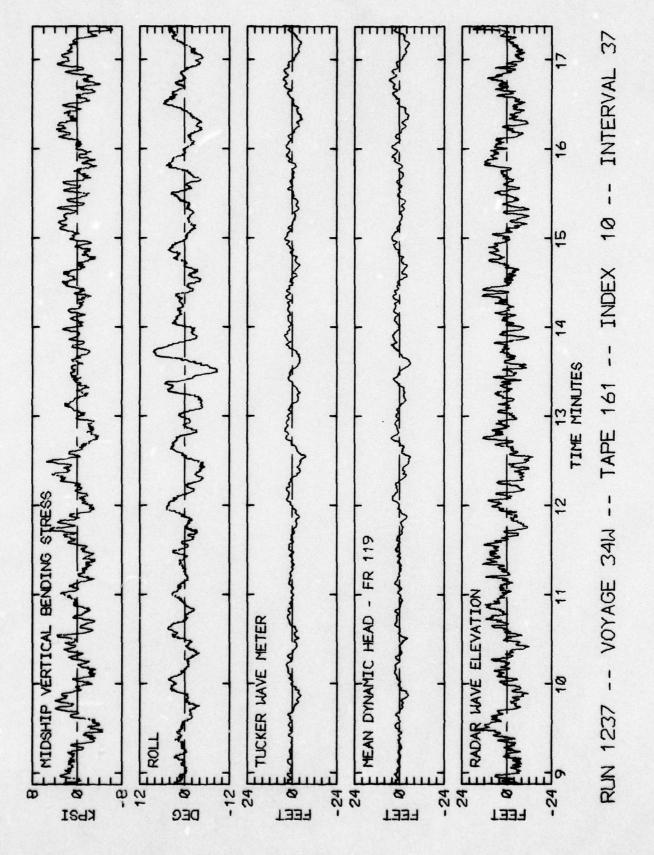
SPECTRUM

33 INTERVAL -- 6 INDEX 1 RUN 1233 -- VOYAGE 34W -- TAPE 161





37 INTERVAL 10 --INDEX 1 **TAPE 161** 1 34M VOYAGE 1 RUN 1237

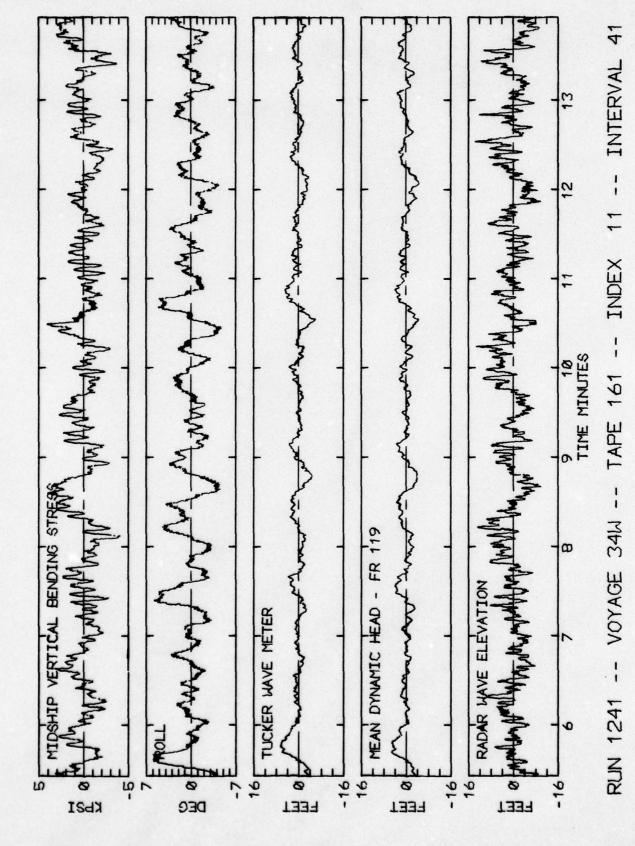


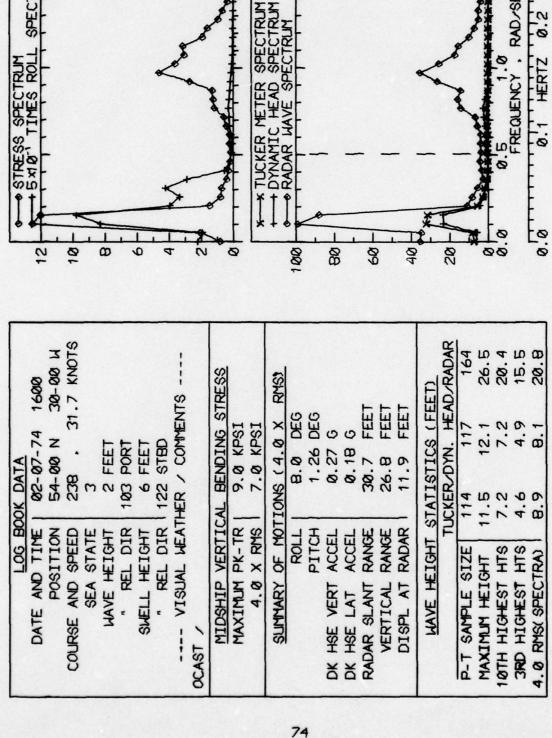
12 + 5 x 0 1 TIMES ROLL SPECTRUM	80 0 4 N	*** TUCKER METER SPECTRUM *** TUCKER METER SPECTRUM *** DYNAMIC HEAD SPECTRUM *** PADAR MAVE SPECTRUM	200	30 W S FREQUENCY . RAD/SEC
DATE AND TIME 02-07-74 1200 POSITION 54-00 N 30-00 W COURSE AND SPEED 241 , 31.6 KNOTS	TH 12	TICAL BENDIN TR 6.7 KP TS 5.8 KP TOTIONS (4.8	DK HSE VERT ACCEL DK HSE LAT ACCEL DK HSE LAT ACCEL DK HSE LAT ACCEL O. 18 G O. 20 G RADAR SLANT RANGE VERTICAL RANGE DISPL AT RADAR 7.7 FEET	MAVE HEIGHT STATISTICS (FEET) TUCKER/DYN. HEAD/RADAR 179 101 107 HIGHEST HTS 6.3 6.6 14.3 3RD HIGHEST HTS 4.2 4.6 11.5 4.0 RMS(SPECTRA) 8.7 8.1 17.7

12.49 1989 1989

146

INDEX 11 -- INTERVAL 41 RUN 1241 -- VOYAGE 34W -- TAPE 161 --



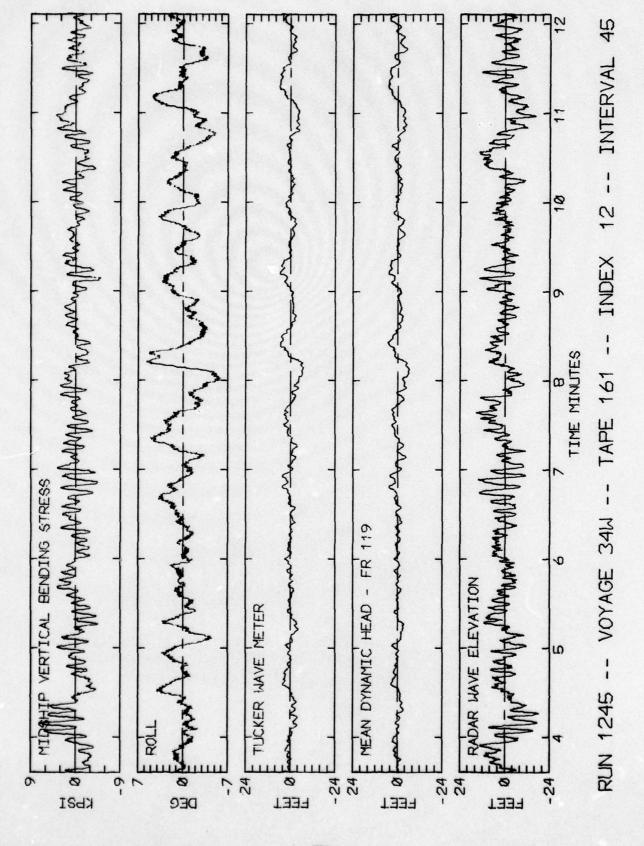


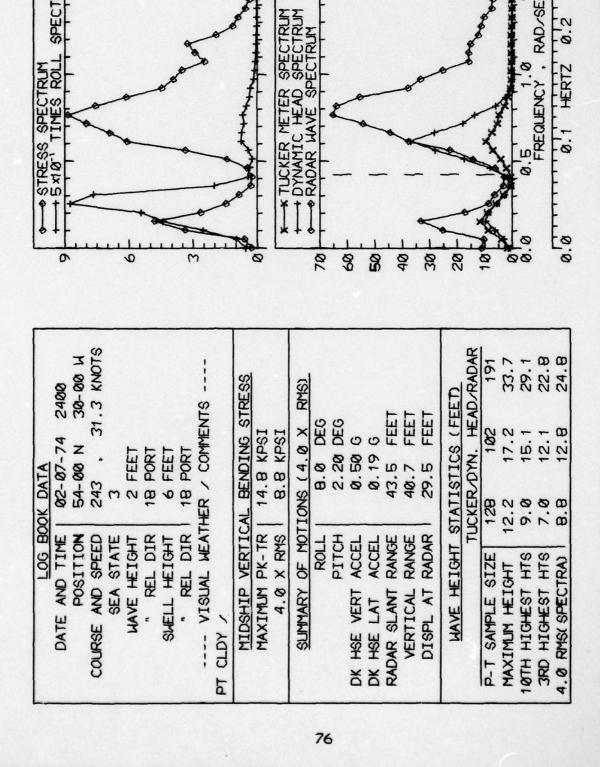
23.45 23.45 24.05 24.05 24.05 24.05 24.05 24.05 25.05

\$ 60 E

SPECTRUM

45 INTERVAL 12 --INDEX 1 **TAPE 161** 34W --VOYAGE 1 RUN 1245



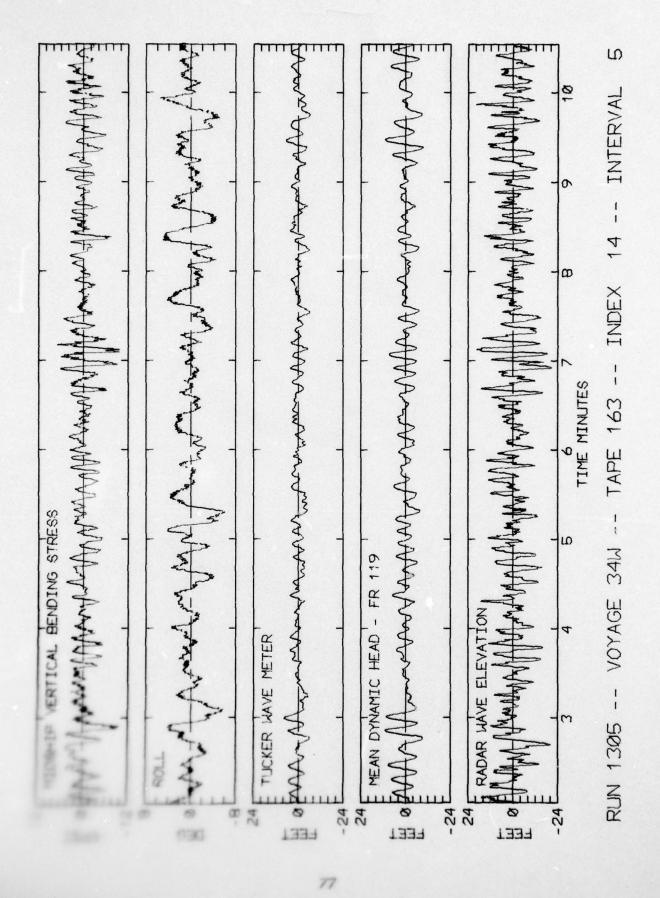


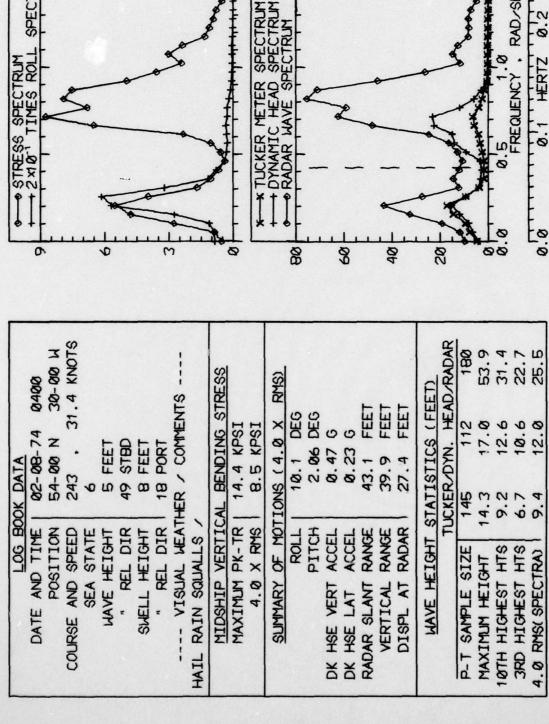
38 58 58

SPECTRUM

10 INTERVAL TAPE 163 -- INDEX 14 --VOYAGE 34W --1 RUN 1305

6.3





SPECTRUM

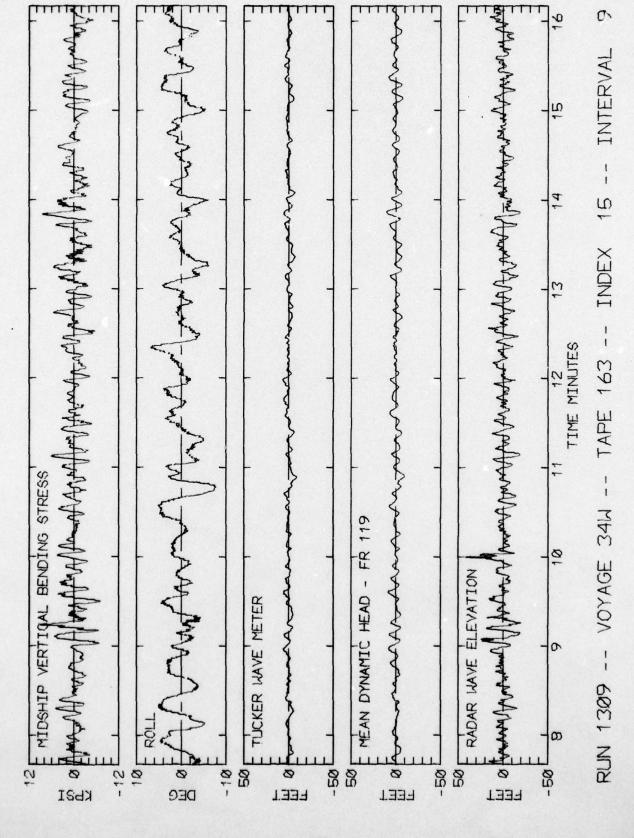
6.3 HERTZ

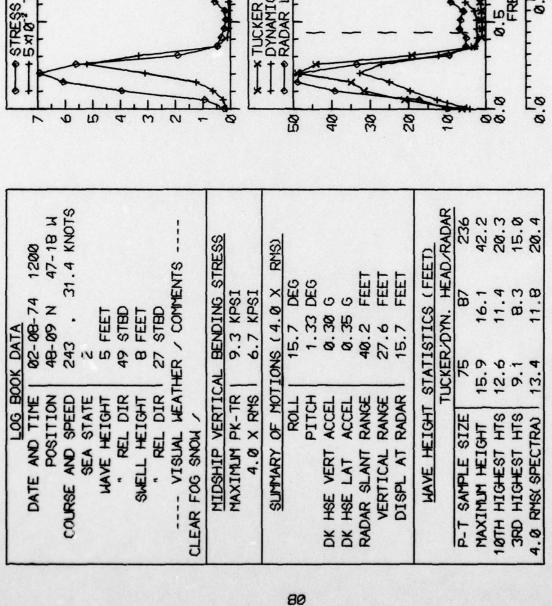
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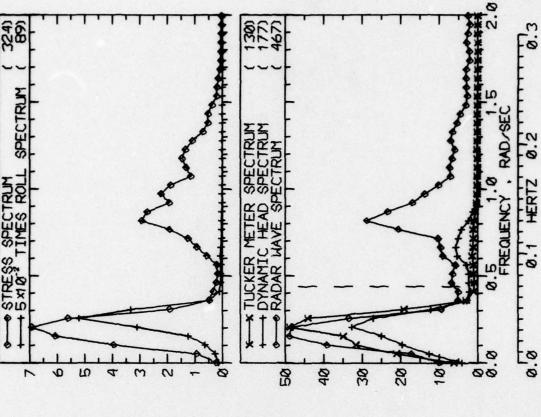
INTERVAL

15 --

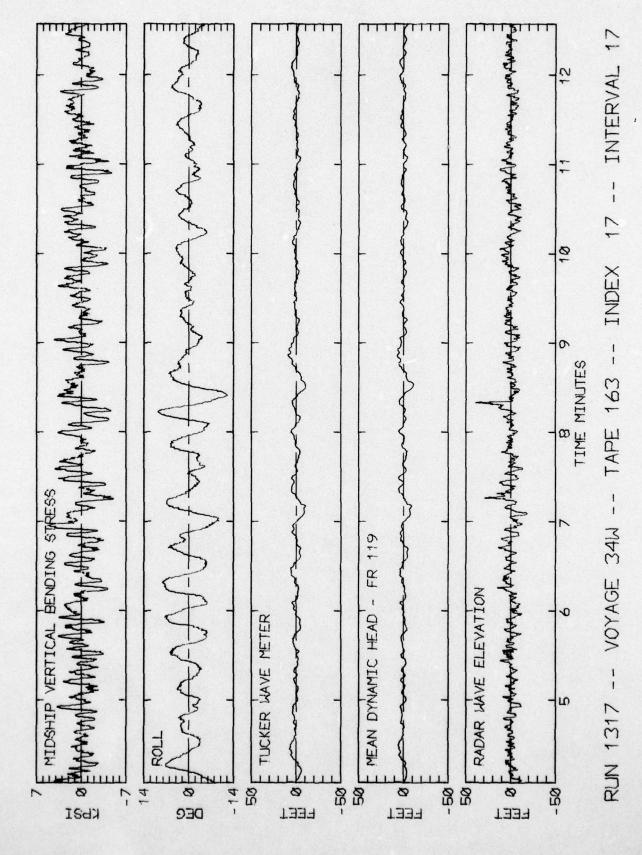
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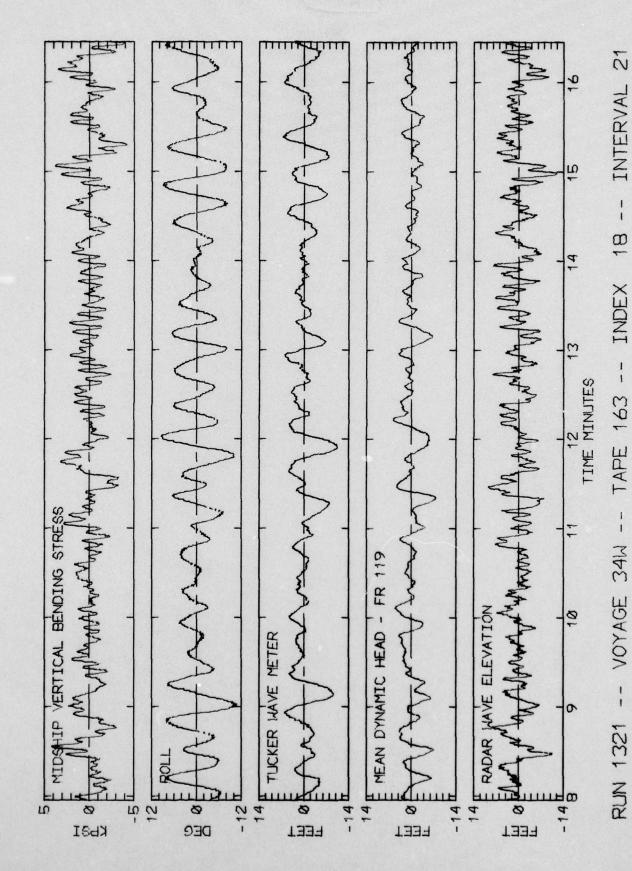
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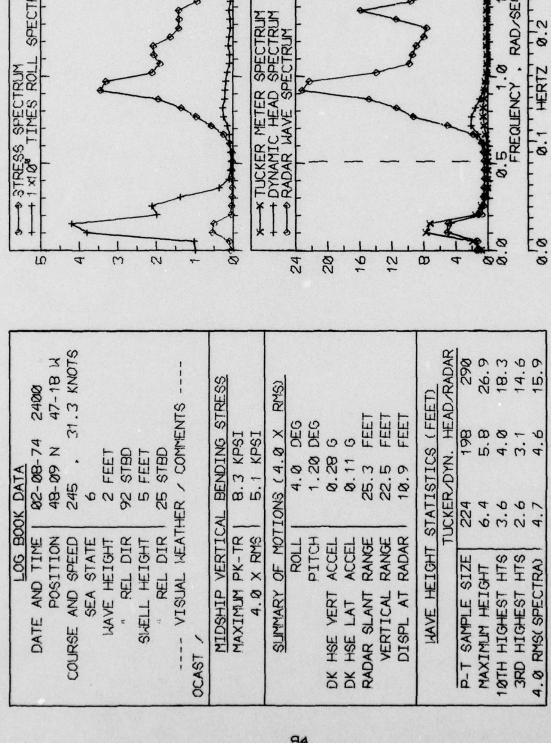


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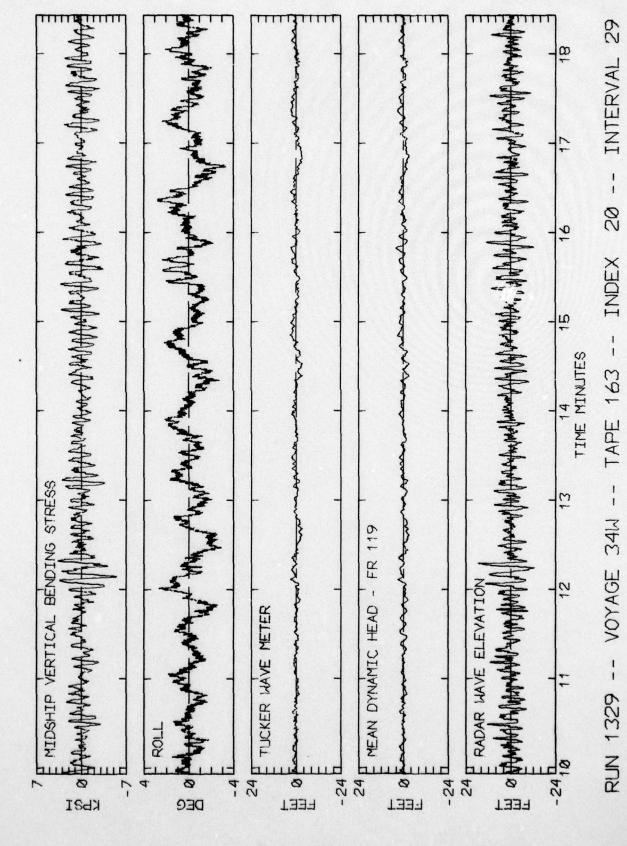


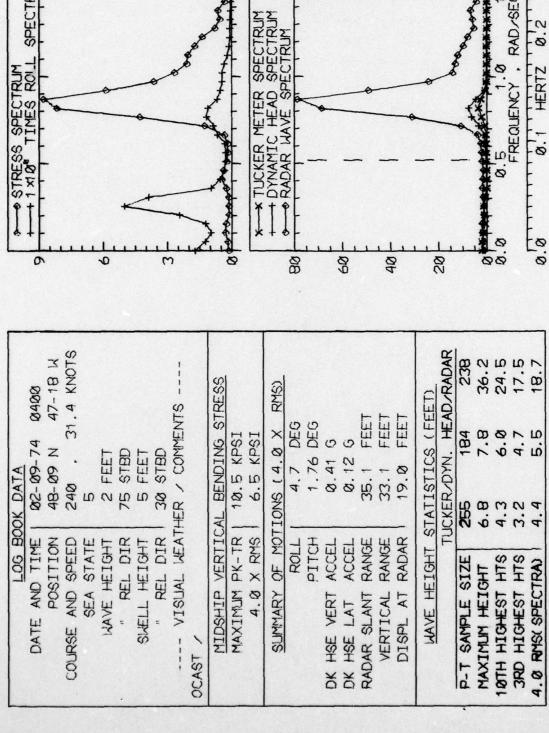


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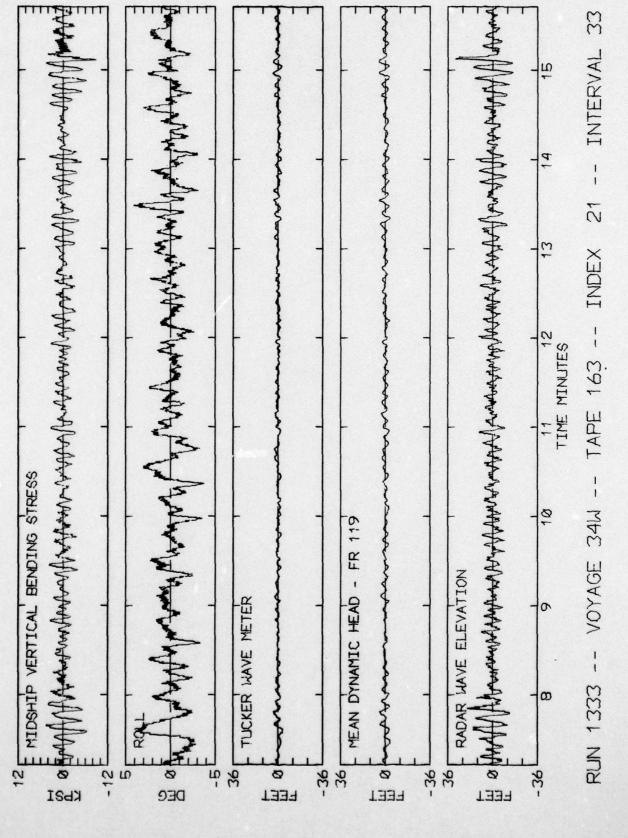


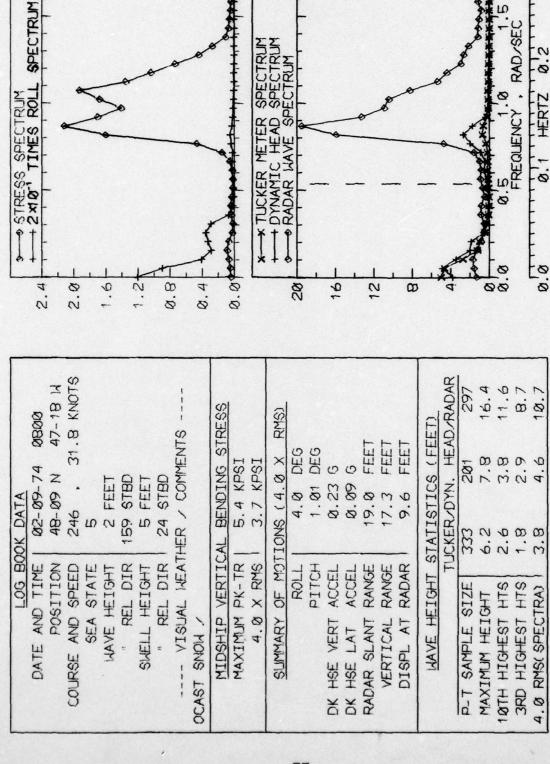


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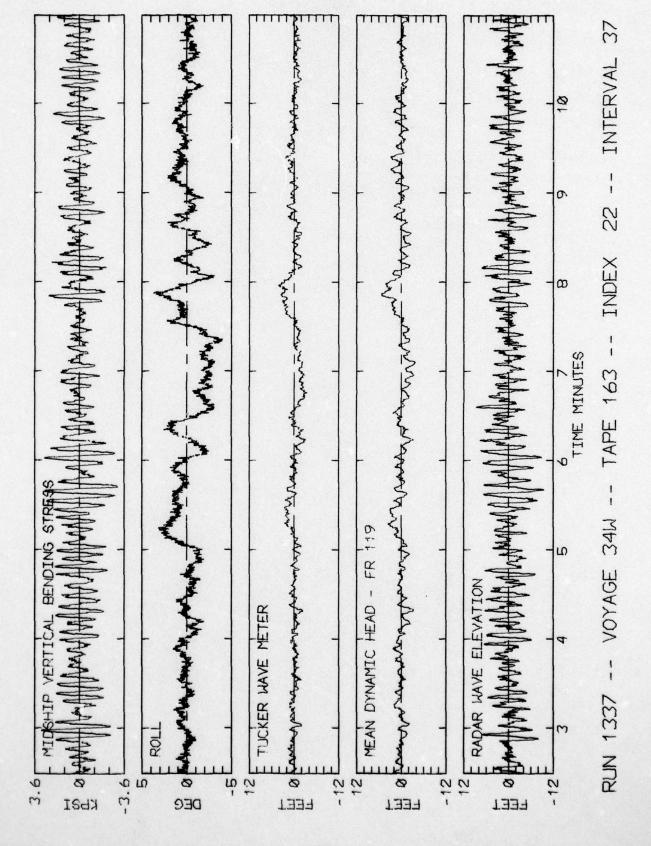
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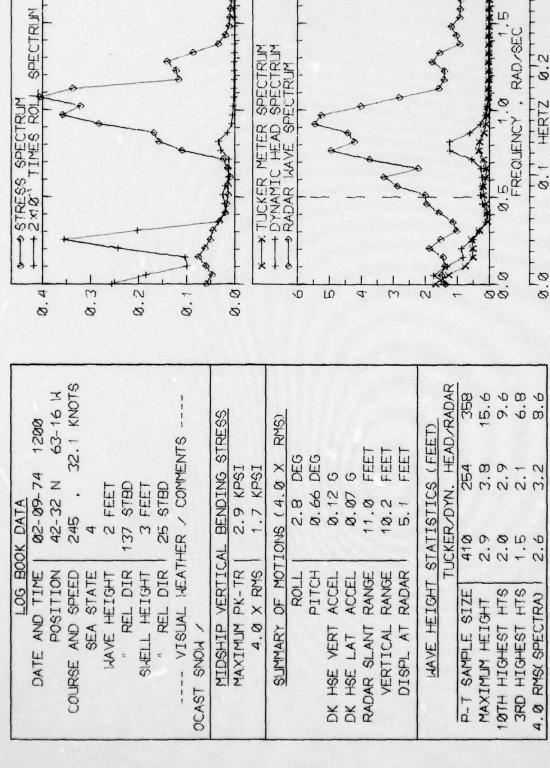
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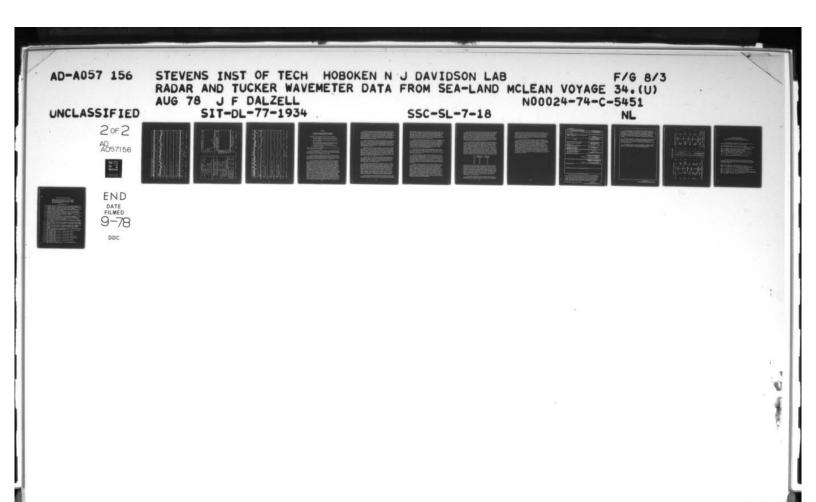


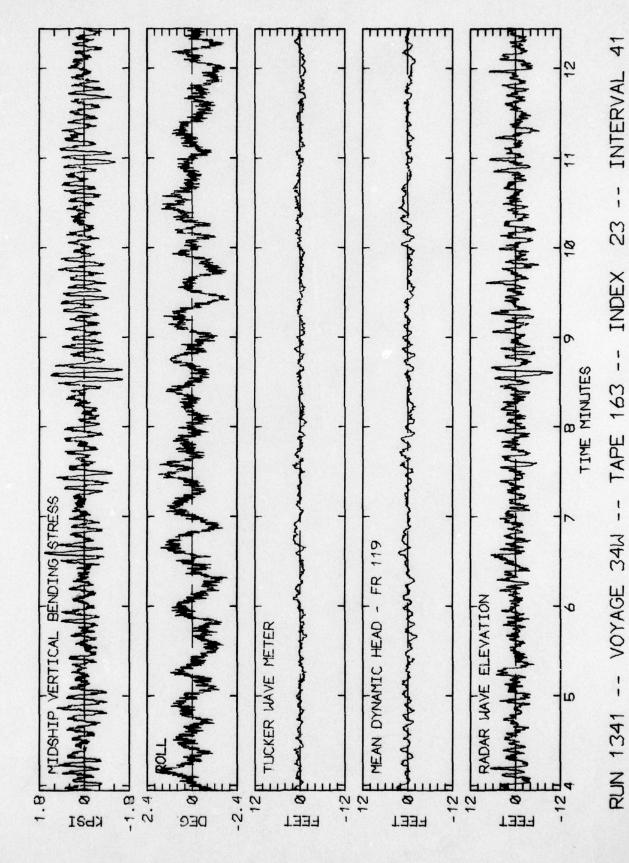


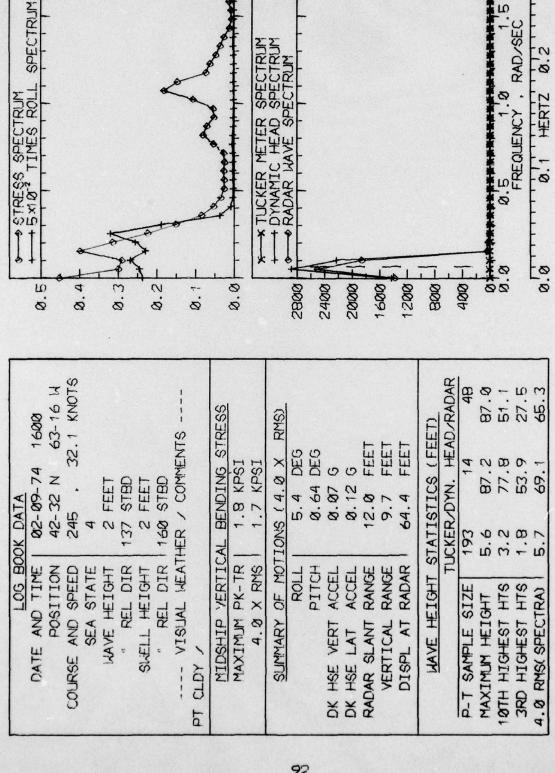
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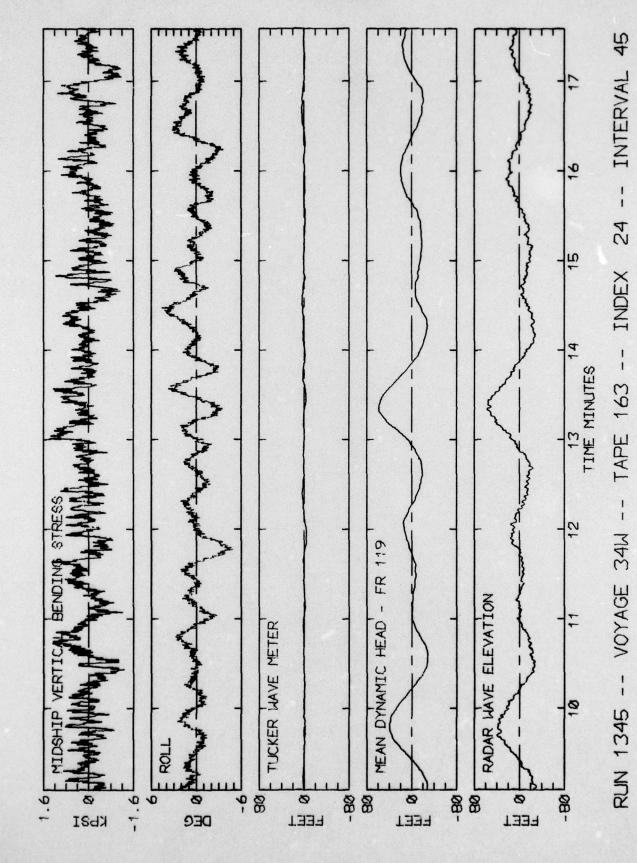
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45 INTERVAL 24 --INDEX VOYAGE 34W -- TAPE 163 --RUN 1345 --



APPENDIX

THE DATA REDUCTION AND PRESENTATION PROCEDURE ACCORDING TO THE DEVELOPMENT IN REFERENCE 4

The data reduction procedure for each interval involved:

- a. Four main computation programs, the last one of which produced a complete file of results for each interval.
- b. Two lister programs to supply immediate indications of some of the results.
- c. One file consolidation program which produced one file for each voyage leg containing everything but the time histories of radar wave and mean dynamic head.
- d. Two programs to generate the final graphical presentations for each interval.

Items b through d amount to bookkeeping operations. The work was done in the four main computation programs.

The first computation program carried out the procedure described in Reference 4 for the radar. At its conclusion the radar wave spectrum and the computed time history were written in temporary files as was the time history of vertical displacement at the radar.

The second program involved reduction of the Tucker data. Both the original data and the displacement file produced by the first program were accessed. The procedure was carried out so that time histories of mean dynamic head and the Tucker Meter signal were available. These were spectrum analyzed, and all results written in a temporary file.

The third computation program accessed the various wave-related time histories (radar, Tucker, and mean dynamic head) and performed a peak-trough analysis on the middle 16-1/2 minutes of each. (Because of the tapering described in Reference 4 both the radar and mean dynamic head data are not valid for the first and last two minutes of sample.) The object of the peak-trough analysis was to produce double amplitude statistics. The zero crossing convention was used; that is, a crest was defined as the largest instantaneous value in an excursion above the sample mean, a trough was the smallest instantaneous value in an excursion below the sample mean. The double amplitude is the difference in elevation between crest and succeeding trough. In this approach small fluctuations are more or less ignored if they are riding on top of large ones. The results resemble the double amplitudes which would be estimated by hand from an oscillograph record except that the hand analyst would probably visually fair through superimposed noise whereas the computer does not. The effect is that while the computer gets about the same number of double amplitudes as the human analyst, the computer's answers tend to be higher if the records are noisy. From the double amplitudes found, the average of 1/3 and 1/10 highest were computed, and the position in the sample of the largest double amplitude was noted. All results, including the actual double amplitudes were written in a temporary file.

The fourth computation program accessed the original data and performed spectrum analyses upon the midship vertical bending stress and roll. It then accessed all previously written temporary files and produced a new file containing all of the results for the interval. These results included log-book data, results of the first analysis of raw data (Ref.3,5), five spectra along with all analysis parameters, all results from the peak-trough analysis, and the two new time histories, the radar wave and the mean dynamic head. These files were meant to be stored on magnetic tape for possible future reference.

The final presentation of results for each interval is contained on two charts. The first type of chart (which appears on the even numbered pages of this report) contains the scalar spectra and a tabulation of results. The second type of chart (odd numbered pages) involves sample time histories. Both are identified at the bottom with the DL run number, the voyage number, the analog tape and interval numbers, and the index number assigned by Teledyne.

Referring to any even page, the tabulation at the left is intended as a summary of the most significant numbers pertaining to the interval. At the top is as much of the original log-book data as it seemed reasonable to squeeze in. This includes date, time, position, and ship speed, as well as the visual estimates of wave and swell heights and directions. Directions are counted from the bow to port or starboard in degrees. The "sea state" is apparently the Beaufort wind. The final line in the first section of the tabulation includes comments on visual weather and, after the slash, any other comment appearing in the log.

The second box in the tabulation involves midship longitudinal stress results. Only two of the many numbers which are available could be included as indices. The first is the maximum peak to trough stress excursion as obtained in Reference 1 or 2. The second index is the significant stress (4 times rms) as derived from the area of the stress spectrum obtained in the present reduction.

The third box in the tabulation is a summary of motions. Again the "significant" motions (4 rms) are indicated. The value for roll was derived from spectrum area, that for pitch and accelerations from the rms of the basic data. (Unless there are significant linear trends in the data the differences are slight between "raw" and "spectrum" rms.) The last three items in the list involve various stages in the radar data reduction. The first is the slant range as recorded. The "vertical range is $R_{\rm c}(t)$ of the radar analysis. This entry is essentially the vertical component of the range relative to the position of the accelerometer package. The number was derived from the spectrum. The last entry is the significant displacement at the radar (significant doubly integrated acceleration). It too was derived from spectrum analyses.

In a sense, the table at the bottom of the tabulation contains the final numerical answers. Items in the first column pertain to the uncorrected Tucker Meter signal. The second column pertains to the mean dynamic

head developed in conjunction with the analysis of the Tucker meter, and the third column pertains to wave elevations derived from the radar system. The first row in the table is the number of double amplitudes found in the middle 16-1/2 minutes of the sample. Below this are noted the maximum height found and the averages of the 1/10 and 1/3 highest double amplitudes. The final line in the table is the significant (4 rms) height derived from the spectral analyses. Ordinarily it is expected that the last two lines of the table will be about the same.

At the right of any even page are plots of the five computed spectra. It was decided to standardize the frequency scale from 0 to 2 rad/sec. In the great majority of intervals everything of interest is contained in this range. In some intervals one spectrum or another is non-negligible beyond 2 rad/sec but nothing much has been seen beyond 2.5 rad/sec for any of the quantities analyzed except in the stress spectrum where something may often be noticed around the frequency of the first mode of vertical vibration. The folding frequency of the analyses is above 20 rad/sec; no aliasing is expected, Reference 3.

The stress and roll spectra are plotted together. The vertical scale is for the stress spectrum. The roll spectrum has been multiplied by the factor noted in the legend before plotting. Dimensions of the stress spectral density are (kpsi²/rad/sec) and those of the roll spectral density are (deg²/rad/sec).

All three wave related spectra (Tucker, mean dynamic head, and radar) are plotted together to the same scale. The dimension of the wave spectral density is (feet 2 /rad/sec). In the wave spectrum plot there is a vertical (slightly joggled) dashed line. This line marks the position of the low frequency cutoff, $\boldsymbol{\omega}_{o}$, discussed in Reference 4 in conjunction with double integration of the vertical accelerations. It is correct to interpret the position of this line as meaning that the double integration has been done correctly for higher frequencies, and incorrectly for lower frequencies.

There are several details about the spectrum analyses which are not documented in the plots because they are constant throughout the data reduction. First, the normalization of the spectra is such that the spectrum area equals variance. All spectra are derived from a Fast Fourier Transform analysis of an 8192 point sample. The fundamental results is 4096 spectral estimates of 2 degrees of freedom each. These estimates are uniformly spaced in frequency at a delta-frequency of 0.00511 rad/sec. In order to improve statistical reliability, the basic spectral estimates were averaged in blocks of 20 estimates at intervals of 10 estimates. The resulting averages are thus equi-speced on the frequency scale at intervals of $\Delta\omega$ = 0.0511 rad/sec. This also means that adjacent spectral estimates as shown in the plot are not quite independent — to about the same degree as spectral estimates from the older autocorrelation methods are not independent.

As a result of the averaging, each spectral estimate has 40 degrees of freedom associated with it. Accordingly, the 90% confidence bounds on the spectra shown in the charts may be formed by multiplying the values given by 0.72 and 1.51. Had the process sampled continued indefinitely and a large number of 20.5 minute samples been obtained and analyzed, nine out of ten of these new estimates of spectral density would be expected to lie within the bounds so constructed. The practical implication is simply that the influence of sampling variability upon the given numerical results is roughly the same as that associated with the result of most other full scale wave measurement exercises.

The last detail of the spectrum analysis is the "total degrees of freedom." This number is included in parentheses at the end of each line of legend because it depends upon the shape of each individual spectrum. It is an estimate of the proper number of degrees of freedom to use in constructing confidence bounds on the sample variance. If each of the numbers in the present 8192 point time histories had been picked randomly the "total degrees of freedom" would be 8191. This is not the case -- adjacent members of all the present time series are highly correlated so that the equivalent "random" sample size is much smaller. In the present data set the "total degrees of freedom" (TDF) is expected to vary between 60 and 600. Approximate 90% confidence bounds on the variances assuming a Normal zero mean process, may be constructed by multiplying the estimate by two factors derived from the percentage points of the Chi-square distribution. Examples of the values of these factors are given as follows:

TDF	Factor for Lower Bound	Factor for High Bound					
60	.72	1.32					
120	.80	1.27					
200	.84	1.17					
400	.89	1.12					
600	.91	1.10					

These are factors for the variances. The square root applies to the rms values so that very roughly the 90% confidence bounds on rms range from the sample rms \pm 15% for TDF = 60 to the sample rms \pm 5% for TDF = 600. The practical implications of these results are quite similar to those mentioned in connection with the confidence bounds on the spectra. There is only so much "precision" obtainable from one 20 minute sample of wave elevation -- that which was attached in the present work appears comparable to that achieved in the past in similar studies. With respect to comparisons between wave meters or between data and predictions of rms ship responses there can be little justification to a concern about differences of 5 to 15% magnitude.

The sample time histories on the odd numbered pages need little explanation, except perhaps to say that the duration of the sample shown (8-1/2 minutes) was a compromise between a desire to display as much of

the 16-1/2 minutes of derived wave time histories as was possible in one page; and the desire to spread the time scale out so that individual fluctuations were visible for intervals involving high ship speed in head seas. To produce the charts an 8-1/2 minute portion of the available 16-1/2 minutes of sample was chosen such that the largest radar wave double amplitude is shown -- as well as (if possible) the largest mean dynamic head double amplitude.

It may be fairly asked why the effort in producing plotted time histories for each interval was considered worthwhile. The answer to the question is fairly simple. While the present data in its original analog form has been scanned systematically by eye, the process involved oscillograph records with a time scale of about 15 minutes to the inch. At this time compression only a gross idea of what was happening can be formed, no detailed assessment of the believability of the data can be made, and, most importantly, the odd malfunction which is enough to upset the spectrum estimates or the statistics may often go unnoticed. This last is considered most important in the radar data. It was pointed out in References 3 and 5 that an attempt was made to weed out intervals where the radar had evidently lost signal and re-established a new reference range. In this process only the most obvious instances could be identified; no guarantees could be made that all instances of moderate or small magnitude had been eliminated.

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J. F. DALZELL	N00024-74-C-5451
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Washington, D.C. 20362 14. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office Ship Structure Committee U.S. Coast Guard Headquarters Washington, D.C. 20590	98 18. SECURITY CLASS. (of this report) UNCLASSIFIED 15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
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So that more precise correlations between full scale observations and analytical and model results could be carried out, one of the objectives of the instrumentation program for the SL-7 class container ships was the provision of instrumental measures of the wave environment. To this end, two wave meter systems were installed on the S.S. SEA-LAND McLEAN. Raw data was collected from both systems during the second (1973-1974) and third (1974-1975) winter data collecting seasons.

It was the purpose of the present work to reduce this raw data, to develop and implement such corrections as were found necessary and feasible, and to correlate and evaluate the final results from the two wave meters. In carrying out this work it was necessary to at least partly reduce several other channels of recorded data, so that, as a by-product, reduced results were also obtained for midship bending stresses, roll, pitch, and two components of acceleration on the ship's bridge.

As the work progressed it became evident that the volume of documentation required would grow beyond the usual dimensions of a single technical report. For this reason the analyses, the methods, the detailed results, discussions, and conclusions are contained in a series of ten related reports.

This report is one of the six in the series in which the detailed results of the data reduction process are presented. Included in this report is the reduced data from the Second Season Voyage 34.

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